

# Team 05: High Speed Motor Test Stand

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Chapter One: EML 4551C

1.1 Project Scope

Danfoss is tasking Team 05 with designing a system that can measure motor efficiency at

standard operating speeds for motors inside various Danfoss Turbocor compressors. Team 05

will determine the best way to measure output power for efficiency calculations and the best way

to couple the motor shafts for operation at high speeds. They will design and implement a safety

shield in order to maintain safe operating conditions while testing the system

Only the Danfoss facility will use the motor testing system. The assembly line will not

use the system to test each compressor; instead, the research and development team will utilize

it. The stakeholders include Danfoss, research, and product development.

1.2 Customer Needs

Danfoss Turbocor research and development team requires a high-speed motor testing

system capable of measuring the power output and efficiency of the Turbocor compressors. The

system will operate at a range of 13,000 to 40,000 rpm. Improvements are to be made to the

existing system based off of need when testing. The system will have a stand since the current

motor testing system sits on the floor. It will also need some sort of structure surrounding the

entire system for safety purposes. Finally, the team will select and add a torque transducer to the

test stand to accurately measure the efficiency of the compressor.

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### **1.3 Functional Decomposition**

From the project scope and customer needs, the Danfoss High Speed Motor Test Stand Team can determine the functions of the stand. The team decides on three main functions. The high speed motor test stand will measure motor efficiency, hold the weight of the motor testing system, and protect the operator from harm while testing is in progress. Each of these main functions will also have subfunctions, which will be discussed below.

A subfunction is what needs to be done in order for the main function to take place. For the test stand to be able to measure motor efficiency, it will first need to be able to operate at standard motor speeds. For the motors used in this project, standard motor speed is between 13,000 to 40,000 rpm. Then, it will have to measure torque with a torque transducer.

To hold the weight of the motor testing system, the stand will need to be built with a suitable material. It will also maintain stability.

A safety shield will attach to the motor test stand to protect the operator during testing. The safety shield will be built with a suitable material. After the safety shield is built, the stand will have easily accessible E-stops added to it.

# **1.4 Target Summary**

After defining our functions and their subfunctions, the Danfoss High Speed Motor Test Stand team can now establish the targets for each subfunction. By establishing targets for the project, it will help the team in the further stages of the design process because they will have clear goals to aim for, and it will help eliminate concepts. Each subfunction discussed in the previous section will have a target that the design must satisfy.

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The first main function for the high speed motor test stand, as discussed above, is to measure motor efficiency. This function has two subfunctions: operate at standard operating speeds and measure torque with a torque transducer. The standard operating speeds of a Danfoss compressor can range from 13,000 to 40,000 rpm; however, the target for this subfunction is 7,000 to 40,000 rpm. This is because the previous Senior Design Team that worked on this project only achieved 7,000 rpm, and one of the goals set by our sponsor is to achieve a speed higher than the previous team (Aponinuola, De La Rose, Jurko, & Pullo, 2017). To measure torque, the torque transducer must be able to measure a torque of up to 100 newton meters and be able to operate at 40,000 rpm.

From the Functional Decomposition, the second main function is to hold the weight of the motor testing system. This function also has two subfunctions. To be able to hold the weight of the motor testing system, the stand must be built with a suitable material and be able to maintain stability. The material used for the test stand must be able to withstand the weight of two Danfoss compressors, which total 272 kilograms. The stand must also maintain stability while operating underneath the weight of the system. If the system is unstable, the two compressor motor shafts become misaligned, and when the misalignment is too great the compressors completely shut down. This shutdown occurs when the radial force exceeds 890 newtons.

Safety of the operator using the high speed motor test stand is one of the main concerns of this design project; therefore, the third main function is to protect the operator while testing is in progress. To protect the operator, the system will have a safety shield which must be at least 0.61 meters long, 0.61 meters wide, and 0.5 meters in depth in order to cover all moving parts of

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the high speed motor testing system. The safety shield will need to be built with a suitable material that can handle the impact energy of a projectile hitting it. Team 05 calculates this energy using the equation below.

$$E = \frac{1}{2}mv^2$$

The variable 'm' represents the mass of the projectile, and 'v' represents the velocity of the projectile. For the worst-case scenario, the team uses the coupler, with an outer diameter of 0.08128 meters and a mass of 0.907 kg, as a possible projectile and 40,000 rpm to calculate the velocity. By converting the revolutions per minute to radians per second and then multiplying it by the radius of the coupler, the velocity of the projectile is 170 meters per second. From the energy equation above, the impact energy of the coupler is 13 kilojoules. The material used must be able absorb an impact energy of 13 kJ. The stand will also need accessible E-stop buttons. An E-stop is defined as "a function that is intended to invert harm or to reduce existing hazards to persons, machinery, or work in progress" (Nix, 2017). For each operator station that can produce mechanical motion, there must be one emergency stop function (Nix, 2017). Finally, for the testing system to be safe to operate, it must prevent the operator from handling the tester while testing. OSHA standards state that rotating parts cannot come into contact with any part of the body. The target set for this subfunction is 0.172 meters because that is the average size of a woman's hand. Team 05 uses this metric because a woman's hand on average is smaller than a man's, and a hand is the most likely body part to come into contact with the tester. The safety shield must be designed so that no operator can come within 0.172 meters of the motor shaft.

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The Target Catalog, Table 2 shown in Appendix C, shows all the metrics discussed above. The table also contains the relating subfunctions and main functions.

# 1.5 Concept Generation

Table 1
System and Concept Description

System	System Title	Concept	Concept Title
	Motor Torque	Concept 1.1	TMHS 311 Torque Transducer
		Concept 2.1	TMHS 310 Torque Transducer
System 1		Concept 3.1	UTM II - 100 Nm Torque Transducer
		Concept 4.1	Froude AG80 Dyno
		Concept 5.1	PCB Rotary Transformer
	Coupling System	Concept 1.2	Zero Max Double Clamp A1C Coupling
System 2		Concept 2.2	Custom Zero Max Carbon Fiber Coupling
		Concept 3.2	SU 90-6 Coupling
System 2	Safety	Concept 1.3	Frame over Rotating Parts
System 3		Concept 2.3	Frame over Entire System
System 4	Frame Adjustments	S Concept 1.4 Alignment Set-Screws	

#### System 1.

One of the high speed motor test stand functions, mentioned in the Functional Decomposition, is to measure motor efficiency. To measure motor efficiency, motor torque will need to be measured. There are two fundamental ways that torque can be calculated. One way is called the indirect method. This typically involves doing a calculation based on the theoretical operation of the system. For example, given a gear train with an input shaft and output shaft, the indirect method would use the input torque and gear ratio to calculate the output torque. Another way is called the direct method. The direct method involves some direct measurement of the

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torque applied by the output shaft of the motor. With this method, the torque is transduced by attaching a resistive sensor to a shaft that is then coupled with the motor shaft (Schicker & Wegener, 2002).

#### Concept 1.1

One way to measure the motor efficiency is to use a torque transducer. Team 05 will research multiple torque transducers because the sponsor desires to measure motor torque using a torque transducer. An important consideration when choosing a torque transducer is the mechanical design of the transducer. Since the compressor motor is a high speed motor, a transducer that uses non-contact bearing should be chosen. Otherwise, the bearings would have to be replaced often which would become a maintenance burden under continuous operation. The high speed of the motor places another, less restrictive, constraint on the selection of a torque transducer. The standard method of a signal transmission in a torque transducer is through use of a slip ring, where the electrical signal is conducted through a rotor by brushes that are in physical contact with the rotor as it spins. A transducer that conducts the signal using a slip ring would likely wear prematurely, and thus should be avoided if possible. Other technologies exist that use contactless conduction for the electrical signal and would require less maintenance. One possible torque transducer for this project is the TMHS 311 from Magtrol, represented by Figure 1. This in-line rotary torque transducer is capable of rotary speeds of up to 32,000 rpm and is rated for a torque of 100 Nm. It has non-contact bearings with a non-contact conduction technology suited for high speed operation. This option would provide a fixed center for the test stand. In hopes to eliminate fighting between the compressors, this option allows each compressor a level of independence that is only possible with a fixed toque transducer. The vibrations from one

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compressor will no longer be transferred to the other compressor. Instead, it will only be fighting against the fixed torque transducer. The only limitation this torque transducer has is that it is only rated to 32,000 rpm. Although that is slightly lower than the max achievable speed by the compressors, it should be suitable for our testing. As you increase rpms, the torque rating of the transducers goes down. This option provides the highest rpm while maintaining the required torque rating that the compressors can reach. This torque transducer can be attached to a fixed mount or adjustable mount. With a fixed mount, the alignment of the shafts could become increasingly difficult if the height is not perfect when machined and manufactured. The assembly is much easier than an adjustable mount, and it takes less time to set up. The fixed mount is also very rigid which means that small vibrations from the compressors will not affect the torque transducer's alignment. With the adjustable mount, the aligning the transducer with the motor shaft will be simpler than with the fixed mount, maintaining that the adjustable mount is level. The adjustable mount design can be seen below by Figure 2.

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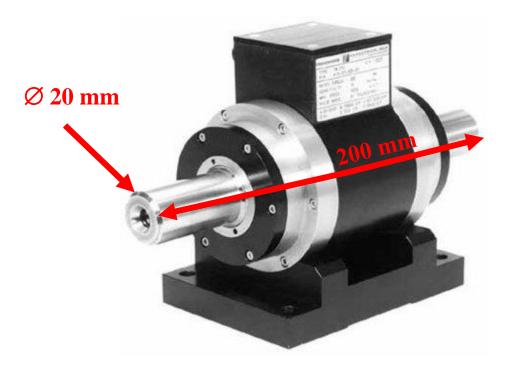


Figure 1. TMHS 311 Torque Transducer.

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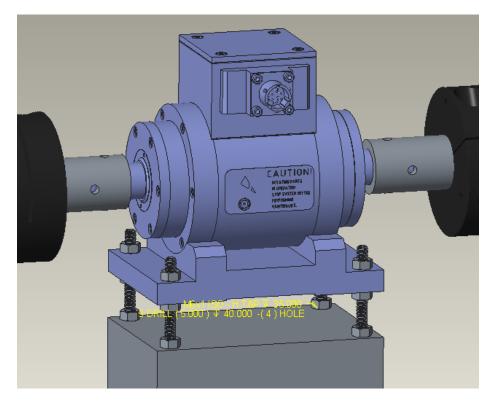


Figure 2. Adjustable mount design

# Concept 2.1

The second torque transducer option is the TMHS 310 also by Magtrol. Similar to the transducer mention in Concept 1, it is an in-line rotary torque transducer that is capable of rotary speeds of up to 32,000 rpm and is rated for a torque of 50Nm. This option is the cheaper version of Concept 1, offering many of the same advantages. This transducer also has non-contact bearings with a non-contact conduction technology suited for high speed operation. While this is the cheaper option, its torque rating falls short of the max torque achievable by the compressor. This was provided as a cheaper alternative to the sponsor by last year's senior design team; however, it was never purchased. This transducer can also be mounted with a fixed or adjustable amount, which is explained above in Concept 1.

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# Concept 3.1

Another possible transducer is the UTM II – 100 Nm by Unipulse, represented by Figure 2. This option provides the team with an alternative to the fixed transducer. Previous teams had issues with vibrations when running the test at higher speeds. With the proper alignment, it is possible that this option could be feasible. The UTM II can reach speeds of 15,000 rpm and is capable of readings up to 100 Nm. One major benefit of this option is that it eliminates the need for a torque transducer mount, as this sensor rotates freely due to its no slip ring. Shown by the schematic represented by Figure 3, the torque transducer is floating, as it is connected on each side by just the flexible couplers. This option still presents a risk of compressor vibrations being transferred between compressors, which can cause fighting between compressors and the testing system to shut down.



Figure 3. UTM II – 100 Nm Torque Transducer.

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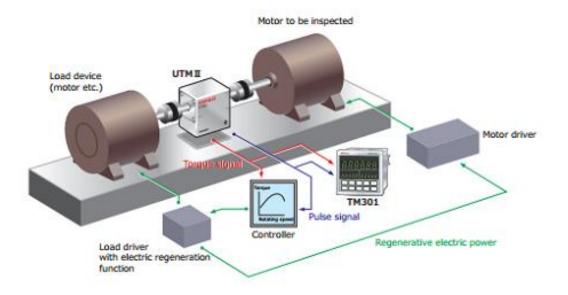


Figure 4. Schematic of the UTM II – 100 Nm Torque Transducer

# Concept 4.1

Another idea to measure the motor efficiency is to use a car dyno. This would replace using another compressor as the generator. The dyno is designed to test electric motor rigs making it ideal for this application. The specific model Team 05 is discussing is the Froude AG80 dyno shown in Figure 5. The steel shaft is supported on deep grove ball bearings which are grease lubricated, and the heat is dissipated by a water cooling system integrated within. It uses twin magnetizing coils that are used to create a magnetic field which absorbs torque. This specific model, the AG80, can handle up to 30 kW of power, 95 Nm of torque, and can spin up to 14,000 rpm. It would bolt directly onto the compressor motor shaft. Instead of having two motors coupled, only one motor would couple to the dyno.

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Figure 5. Froude AG80 dyno.

# Concept 5.1

The final concept to measure motor efficiency is to utilize a rotary transformer. Like the previous concept, the transformer would function as the generator for the compressor motor instead of another compressor. A rotary transformer works similar to a regular transformer by having primary and secondary coil windings separated into two cores. The magnetic flux created in the two cores results in a torque measurement. The transformer has a flange with splined shaft which allows for easier coupling. It can be bought with a speed sensor as it can be a 2 in 1 system. The model the team is considering is the PCB Piezotronics 4115k-04A shown in Figure 6. The maximum torque this motor can handle is 55 Nm and has an overload limit of 170 Nm, and it has a maximum speed of 15,000 rpm.

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Figure 6. PCB rotary transformer.

# System 2.

Both the 2016 and 2017 design teams looked into the coupling system. The coupling system is the method in which the motor shafts of the two compressors are attached. Both teams chose a coupler, but this year's team will further research couplers to find out if there are better options.

# Concept 1.2

The Zero Max Double Clamp A1C Coupling, Figure 7, was selected by the 2017 senior design team for a variety of reasons. This model can reach speeds of up to 15,000 rpm. While it is not capable of reaching the desired speed of 40,000 rpm, the sponsor wants the team to start testing with this coupler to ensure that the method to measure motor torque is viable. The Double Clamp A1C model is a variation of a composite disc coupling, otherwise known as an Oldham coupling. Oldham couplings are made up of three discs which are joined by a tongue and groove joint. Tongue and groove joints are used to join two bodies together. The groove is a slot along one edge of the body, and the tongue is a ridge that is a little less than the depth of the groove.

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The middle disc rotates about the center of the input and output discs and, in this case, contains springs which are used to reduce the backlash of the mechanism. Because of this configuration, the Double Clamp A1C can tolerate up to 2 degrees of angular misalignment, 0.44 mm of parallel misalignment, and 1.6 mm of axial misalignment. At the minimum bore size, it's weight is 0.3 kilograms. This is very light and could reduce the vibrations in the system.



Figure 7. Double Clamp A1C Coupling.

# Concept 2.2

Another option would be a coupling made of carbon fiber. Zero Max is willing to make the team a custom-made carbon fiber double clamp coupling. The carbon fiber coupling would be able to reach speeds of 40,000 rpm and would be able withstand the high speeds and high torque. It would be another variation of an Oldham coupling and would cost around \$2,000. This model would ideally be able to tolerate the same amount of angular, parallel, and axial

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misalignment as the A1C. The carbon fiber model would also be lighter than the Double Clamp which would assist with vibrational issues from slight misalignments.

# Concept 3.2

The SU coupling, represented by Figure 8, is another form of disc coupling. It is torsionally rigid, which eliminates backlash and doesn't require any lubrication or maintenance. The couplings come in multiple sizes. The 90-6 size meets most of our goals. It is capable of withstanding 480 Nm of torque, satisfying the requirement of 100 Nm. It has a maximum balanced speed of 22,700 rpm, which is below our goal of 40,000 rpm. It can tolerate 0.75 mm of axial misalignment and 1.5 degrees of angular misalignment, which are within our sponsors requirements of 0.5 mm of axial misalignment and 1 degree of angular misalignment. It does not accommodate parallel misalignment. It has a weight of 1.54 kilograms which could substantially affect the vibrational issues in our system.



Figure 8. SU coupling.

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### System 3.

Safety of the operator is very important to consider when designing this test stand. Without certain safety precautions, handling a machine with an exterior motor shaft that can reach speeds of 40,000 rpm can lead to serious injury. The High Speed Motor Test Stand Team will design a safety shield to make the tester safe to operate.

### Concept 1.3

One option for the safety shield is to use a frame that only covers the moving parts of the motor testing system, mainly the rotating motor shaft. Figure 9 further shows this concept. The team has multiple ideas to gain access to the tester covered by the safety shield. The shield can be free standing, meaning that it is not attached to anything. This allows for the individual using the tester to simply lift the shield off the system if they need to access any parts beyond it. The team will have to design the shield to be lightweight so the operator can easily lift it. If the shield is bolted down, possibly to the frame or the stand, the shield can have a door on the front for accessibility. The door can be a sliding door or a hinged door. The shield can be made of multiple materials including wire mesh, acrylic glass, and polycarbonate. Most wire mesh used to guard machinery are constructed with 10-gauge wire, which can handle a load of about 1,500 newtons. Acrylic glass is often chosen over regular glass in applications where non-shattering is desired. Acrylic glass's impact strength depends on its thickness. Polycarbonate is a great material when a high impact resistance is a requirement. For example, polycarbonate is one of the few materials used for bullet proofing.

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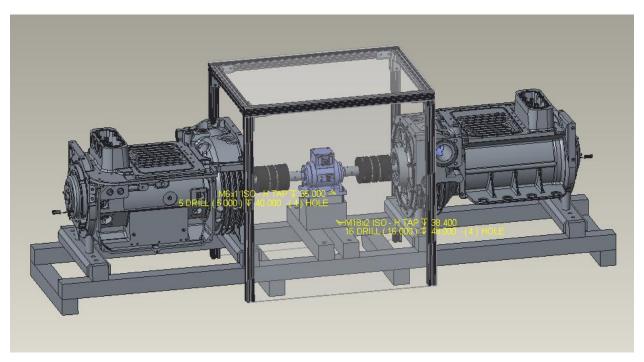


Figure 9. Concept 1 safety shield

# Concept 2.3

Instead of just covering the rotating motor shaft, the safety shield could cover the entire system, including the two compressors, the frame, and the motor shaft. This idea is shown below by Figure 10. This design will be fixed and will have multiple access doors so that the operator can have access to all parts of the motor test stand. While the design shown below has a wire mesh guarding, other materials can be utilized instead. These materials include and they are further discussed above in Concept 1.

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Figure 10. Concept 2 safety shield

# System 4.

The motor testing frame was already designed and implemented by the previous years' senior design teams, but this year's team will most likely need to make adjustments to this frame depending on what motor torque testing device is chosen. The previous senior design team's frame design, Figure 11, used 50.8 mm x 50.8 mm steel tubing and welded brackets with a 3/8-24 tapped hole. A 63.5 mm set screw was used to set the rails, which are connected to the compressor feet, in place in the lateral direction. Adjustments in the 'z' or vertical direction, were accomplished via shims, represented by Figure 12. The overall design proved to work well; however, the shims proved to be marginally successful. Possible changes to the frame design are discussed below.

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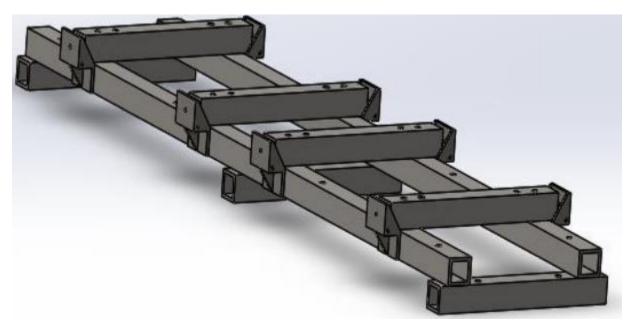


Figure 11. 2017 Senior design team frame design.

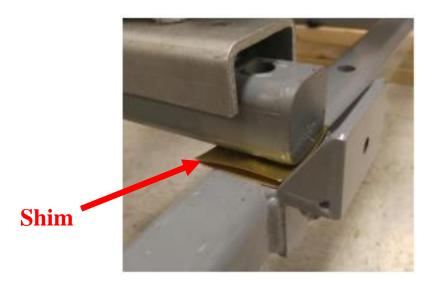


Figure 12. Application of the shim.

# Concept 1.4

One alternative to using the shims is to use set screws to lift the compressor. Team 05 can tap eight holes in the 50.8 mm x 50.8 mm steel tubing support brackets that support the four

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crossbeams which connect to the feet of the compressor. This will allow a new set screw to raise each leg in the z or vertical direction. The crossbeam tubing that connects to the feet of the compressor must also be set in place in the z direction so vibrations don't cause it to move up and down during testing; therefore, there needs to be a way to fasten the cross beam to the support beam either with a bolt and nut or another method of fastening.

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# Appendices

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### **Appendix A: Code of Conduct**

#### **Mission Statement**

The Danfoss High Speed Motor Test Stand Team is dedicated to work together in a positive environment through the entirety of this project. Each team member will always be respectful and professional with other team members. Each member will utilize his or her strengths in order to contribute as much as possible to this project.

#### **Team Member Roles**

# **Team Manager – Emily Simmons**

The Team Manager will ensure that each team member is aware of his or her responsibilities through every stage of the design project. She will also make sure that all members are completing assigned tasks in a timely manner. The Team Manager is responsible for editing each deliverable before the submission deadlines. This includes all reports, presentations, and any other documents required by the project. Once the Team Manager has edited a deliverable, she will be in charge of submitting it on time. Lastly, the Team Manager will always inform the other team members of the project's progress.

#### **Lead ME – David Balbuena**

The Lead ME will be in charge of the technical part of the project. This includes data analysis, programming, and any calculations that need to be done. The Lead ME will be held responsible for these tasks even when the work is done by another team member. In the event that another team member does any calculations, the Lead ME will thoroughly check their work for correctness.

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### **Design Lead & Communication Liaison – Jacob Quigley**

The Communication Liaison will be the main contact between the senior design team and the sponsor. The responsibilities of the Communication Liaison are but not limited to ensuring that the wants and needs of the customer are well understood, ensuring that the sponsor is aware of the current state of the project, and providing the sponsor with feedback and answering/ finding the answers to any questions that may come up.

The Design Lead will be tasked with creatively designing a mounting stand for the torque transducer and its connections. The Design Lead will also ensure that the safety of the test stand is improved. All parts will be made by the Design Lead taking into account the machinability and cost of the process. All part drawings will be done by the Design Lead, and he will schedule drawing reviews with all team members before any submissions or purchases.

#### Financial Planner – McLaren Beckwith

The Financial Planner will be responsible for the supervision of the project's budget as well as maintaining a record of all of the relevant team purchases. All expenditures must be reviewed by the financial planner for approval. Pending approval, the planner is responsible for analyzing alternative products and verifying that the order is satisfactory. Once the transaction is complete, a record of the purchase must be created and maintained by the planner.

# **Web Designer – Charles Daher**

The Web Designer will be in charge of creating the template for the 2017 High Speed Motor Test Rig website. He will update the website as necessary with information describing the project, project deliverables, and sponsor and team member information. He will make sure that

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the website is easy to navigate, esthetically pleasing, and always up to date with the project's progress.

# **Organizational Chart**

Team Member	Team Member Roles					
Names	Team Manager	Lead ME	Design Lead	Communication Liaison	Financial Planner	Web Designer
David Balbuena		<b>&gt;</b>				
McLaren Beckwith					1	
Charles Daher						✓
Jacob Quigley			1	1		
Emily Simmons	1					

#### **All Team Members:**

- Contribute equally
- Listen and be open-minded to others' ideas
- Provide constructive feedback
- Deliver on commitments

# Communication

Communication between team members will be done in person on Tuesdays and Thursdays in class, through a group messaging app called GroupMe, and on Google Drive when preparing presentations and papers that we will all collectively be collaborating on. If a member of the team is having difficulty with communication, (i.e. not responding to messages/ not doing

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their part) Jacob and/or Emily will be tasked with trying to effectively communicate the task at hand. If this is a continuous problem, it will be addressed with Dr. McConomy.

Communication between the senior design team and the sponsor at Danfoss will be done mostly through the Communication Liaison, Jacob. Verbal communications between Jacob and the sponsor pertaining to the project will be relayed to the team members using GroupMe. The Communications Liaison will also handle all emails and will be responsible for sharing the information to all group members.

# **Team Dynamics**

Each team member will have their own responsibilities during the project. They are in charge of making sure their portion of the project is progressing in a timely manner and are ultimately responsible for making sure it is completed by the specified deadline. One of the most important things is that a team member should communicate with the team if they are having difficulty completing a task.

#### **Ethics**

The team will be adhering to the National Society of Professional Engineers' Code of Ethics. Team members are required to model their behavior to the highest standard of honesty and integrity for the benefit of the client, the team and the profession.

### **Dress Code**

During presentations, team members will be expected to dress in business formal attire. Client meetings will be held in business casual attire. There will be no required dress code for routine team meetings. All dress code expectations are subject to change with a unanimous team decision.

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### Weekly and Biweekly Tasks

Weekly meetings will be held between team members during class time. In these meetings, the group will make sure all the team members are up to date on the progress of the project. Project updates and any new information will be discussed here. At least one meeting per week with all team members will be expected with strict attendance. The team will communicate with the sponsor biweekly, either in person or through Jacob Quigley. If needed the team will plan for more meetings depending on the project direction.

### **Decision Making**

All decisions will be made together as a team. Ideally, in the event that two group members disagree, an intelligent conversation would be had including all team members, leading to a resolution. If there is still a disagreement, a vote would be taken amongst team members. We have an odd number of group members so this should solve the issue. In the unlikely event that only a certain amount of team members could vote and it resulted in a tie, the tiebreaker would go to whoever is leading that discipline. For example, if it were a discrepancy on the background color of the webpage, Charles would have final say since he is the Web Designer.

#### **Conflict Resolution**

If the team members have any discord, the following steps will be employed:

- Ideas will be discussed with all members to analyze the pros and cons.
- The leader of each department will decide what the final result will be.
- If needed, the team manager will intervene.
- Instructor will facilitate the resolution of conflicts.

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# **Amendment Process**

This code of conduct can be amended only if all team members sign off on the amendment.

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# **Statement of Understanding**

By signing this document, the members of the Danfoss High Speed Motor Test Stand

Team agree to the code of conducts and understand its principles.

Name	Signature	Date
Emily Simmons	Englio	09/21/17
David Balbuena	Danis Mallen	09/21/17
McLaren Beckwith	MB	09/21/17
Jacob Quigley	150)	9/21/17
Charles Dahn	che der	9/21/17



# **Appendix B: Functional Decomposition**

Table 2 Functional Decomposition

		Main Functions			
		Measure Motor Efficiency	Hold the Weight of Motor Testing System	Protect Operator while Testing	
	Operate at standard motor speeds	•			
S	Attach a safety shield			•	
tion	Measures torque with a torque transducer	•			
Sub-Functions	Build with appropriate material		•	•	
	Add accessible E-stops			•	
	Maintain stability		•		
	Prevents operator from handling tester while testing			•	

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# **Appendix C: Target Catalog**

Table 3
Target Catalog

Main Function	Sub-Functions	Type of Target	Target
Measure motor	Operate at standard motor speeds	Speed	7,000 - 40,000 rpm
efficiency	Measures torque with a torque transducer	Speed, Torque	40,000 rpm, 100 Nm
Hold the weight of	Build with appropriate material	Mass	272 kg
motor testing system	Maintain stability	Radial Force	890 N
	Attach a safety shield	Length	0.61 m x 0.61 m x 0.5 m
Protect operator	Build with appropriate material	Impact Energy	13 kJ
while testing	Add accessible E-stops	Number of E-stops	1 E-Stop
	Prevents operator from handling tester while testing	Length	0.172 m

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