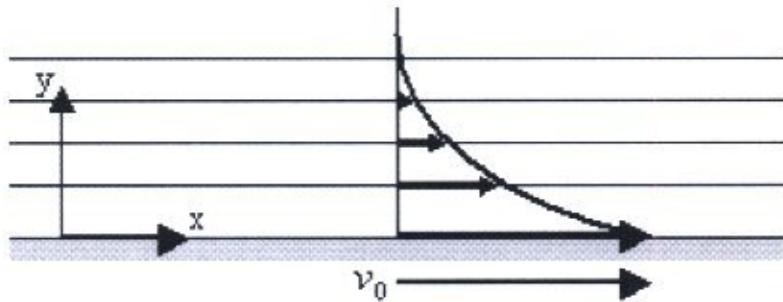


# Stokes First Problem

## 1 Stokes' 1st

Stokes' first problem, also erroneously called Rayleigh flow:



*Continuity:*

$$\operatorname{div}(\vec{v}) = 0 = \frac{\partial u}{\partial x} + \frac{\partial f}{\partial y} \implies u = u(y, t)$$

*y-momentum:*

$$\rho \frac{Df}{Dt} = -\rho g - \frac{\partial p}{\partial y} + \mu \nabla^2 f \implies p = -\rho gy + P(x, t)$$

*x-momentum:*

$$\rho \frac{\partial u}{\partial t} + \rho u \frac{\partial u}{\partial x} + \rho f \frac{\partial u}{\partial y} = -\frac{\partial p}{\partial x} + \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right)$$

The *x*-momentum equation becomes:

$$u_t = \nu u_{yy}$$

where  $\nu = \mu/\rho$  is the dynamic viscosity.

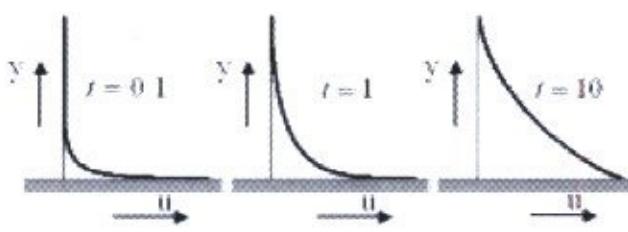
*Simpler way: use dimensional analysis*  
 $\therefore u = f(y, t, \nu, L)$   
 But equation is linear  
 $\therefore u \propto u$   
 $\therefore u = f(y, t, \nu)$   
 choose  $t \geq T$  and  $\nu \rightarrow \frac{L^2}{T}$   
 $y t^\alpha \nu^\beta \rightarrow L T^\alpha L^{2\beta} T^{-\beta}$   
 $\therefore \alpha = \beta = -\frac{1}{2}$

**Exercise:**

How would you normally find  $u$ ?

A simpler way to solve is to guess that the solution is similar: after rescaling  $u$  and  $y$ , all velocity profiles look the same.

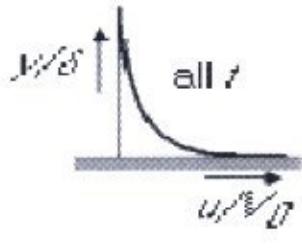
Original profiles:



$$\frac{u}{u} = f\left(\frac{y}{\sqrt{\nu t}}\right)$$

$$\Pi_y = \eta \equiv \frac{y}{\sqrt{4\nu t}}$$

Supposed shape after scaling  $u$  with  $V_0$ , and  $y$  with a characteristic *boundary layer thickness*  $\delta$  that increases with time:



$$\frac{\partial \eta}{\partial t} \propto \frac{\partial \eta}{\partial t}$$

$$f_t = \frac{df}{dy} \frac{\partial y}{\partial t} \\ = \frac{df}{dy} \frac{1}{\sqrt{4\nu t}} \\ = \frac{df}{dy} \frac{1}{4\nu t}$$

Mathematical form of the similarity assumption:

$$\frac{u}{V_0} = f\left(\frac{y}{\delta(t)}\right)$$

The proof is in the pudding; if it satisfies the P.D.E., I.C., and B.C., it is OK.

$$u_t = \nu u_{yy} \implies -V_0 f' \frac{y}{\delta^2} \delta_t = \nu V_0 f'' \frac{1}{\delta^2}$$

$$\frac{(u)}{(u)_t} = \nu \frac{(u)}{(u)_{yy}} \implies \frac{\frac{dy}{dt}}{\frac{dy}{dt}} = -\frac{1}{2} \frac{\eta}{t}$$

Put  $\eta = y/\delta$ :

$$-V_0 f' \eta \frac{\delta_t}{\delta} = \nu V_0 f'' \frac{1}{\delta^2}$$

$$\frac{df}{dy} \frac{df}{dy} \frac{\partial \eta}{\partial t} = \nu \frac{1}{4\nu t} \frac{df}{dy}$$

Separate into terms depending only on  $\eta$  and terms depending only on  $t$ :

$$-\frac{f' \eta}{f''} = \frac{\nu}{\delta \delta_t} = \text{constant} - \frac{1}{2}$$

$$\cancel{\frac{df}{dy} - \frac{1}{2} \frac{\eta}{t} f'} = \frac{1}{4t} f''$$

It does not make a difference what you take the constant; this merely changes the value of  $\delta$ , not the physical solution.

Solving the O.D.E.s for  $\delta$  and  $f$ , we solve the P.D.E. For the boundary layer thickness  $\delta \delta_t = 2\nu$  so

$$\delta = \sqrt{4\nu t}$$

For the velocity profile  $f'' = -2\eta f'$  hence

$$f = \text{erfc}(\eta)$$

$$\text{erf}(1) = -0.8427$$

where erfc is the *complementary error function* defined as

$$\text{erfc}(x) \equiv \frac{2}{\sqrt{\pi}} \int_x^\infty e^{-\xi^2} d\xi$$

$$\text{erf}(1) = 0.16$$

### Exercise:

Derive the expressions for  $\delta$  and  $f$ .

•  
Total:

$$u = V_0 \text{erfc}\left(\frac{y}{\delta}\right) \quad \delta = \sqrt{4\nu t}$$

You should now be able to do 7.14, 16, 17

# Oseen vortex

$t < 0$

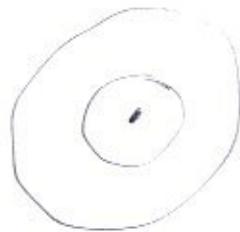
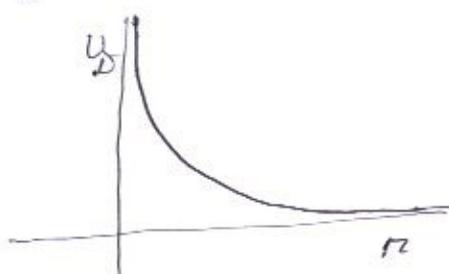
$\Omega \gg 1$



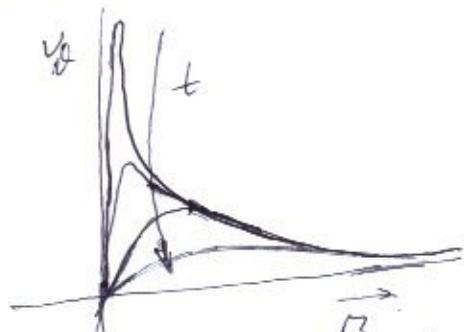
$t = 0$ : stop cylinder

$$\text{velocity field: } \vec{V} = \frac{\Gamma}{2\pi r} \hat{\omega}$$

$$\left( \text{where } \frac{\Gamma}{2\pi\varepsilon} = \Omega\varepsilon \text{ so } \Omega = O(\varepsilon^2) \right)$$



$t > 0$



Linearity

$$v_\theta = \Gamma f(n, t, \alpha)$$

$$\frac{v_\theta}{\Gamma} = f(n, t, \alpha)$$

$$\frac{v_\theta}{\Gamma} = f(n, t, \alpha) L T^{-1} L^{-2} T T^a L^{2\beta} T^{-\beta} \quad \alpha = \frac{1}{2}, \beta = \frac{1}{2}$$

$$\frac{v_\theta}{\Gamma} = \frac{v_\theta}{\Gamma} \sqrt{vt} = f\left(\frac{n}{\sqrt{vt}}\right)$$

$$v_\theta = \frac{\Gamma}{\sqrt{vt}} f\left(\frac{n}{\sqrt{vt}}\right)$$

$f(\alpha) \sim \frac{1}{\alpha}$  large  $\alpha$

$$\frac{v_\theta}{\Gamma} \left[ f\left(-\frac{n}{2t}\right) + f\left(\frac{n}{2t}\right) \right] = \frac{v_\theta}{\Gamma} \left[ n \frac{1}{\sqrt{vt}} + f\left(\frac{n}{\sqrt{vt}}\right) \right]$$

Appendix B  $v_x = v_z = 0$

$$v_{x\theta} = v_{x\theta}(r, \theta) p = p(r, t)$$

$$\text{continuity: } \frac{\partial}{\partial r} r v_\theta = - \frac{dp}{dr}$$

$$x\text{-momentum: } \frac{\partial v_x}{\partial r} = 0$$

$$z\text{-momentum: } \frac{\partial v_z}{\partial r} = 0 \quad \left[ \frac{\partial}{\partial r} \left( r \frac{\partial v_\theta}{\partial r} \right) - \frac{v_\theta}{r^2} \right]$$

$$\frac{\partial v_\theta}{\partial t} = \nu \left[ \frac{\partial}{\partial r} \left( r \frac{\partial v_\theta}{\partial r} \right) - \frac{v_\theta}{r^2} \right]$$

$$\frac{\partial v_\theta}{\partial r} = \frac{\partial}{\partial r} \left( r \frac{\partial v_\theta}{\partial r} \right) - \frac{v_\theta}{r}$$

$$a = \frac{1}{2}, b = \frac{1}{2}$$

$$\frac{n}{D} \frac{d}{dt} \left[ -\frac{1}{2t} f + f' \left( -\frac{1}{2} \frac{\eta}{t} \right) \right] = \frac{P}{\sqrt{Dt}} \left[ n f' \frac{1}{\sqrt{t}} + f \frac{1}{\sqrt{Dt}} - \frac{f}{n} \right]$$

\*  $n\sqrt{Dt}$ :

$$f' - \frac{1}{2} \eta^2 f - \frac{1}{2} \eta^3 f'' = \frac{1}{2} \eta^2 f''' + \eta f'' - f$$

$$f' - \frac{1}{2} \eta^2 f - \frac{1}{2} \eta^3 f'' = (1 - \frac{1}{2} \eta^2) f = 0$$

$$\underbrace{\eta^2 f''' + \eta f''}_{\eta(n-1) + n - 1} - \underbrace{(1 - \frac{1}{2} \eta^2) f}_{\text{or } f = \eta^{-1}} = 0 \rightarrow \frac{1}{\eta} \text{ is a solution.}$$

so by  $f = \frac{s}{\eta}$  to simplify

$$\eta^2 f''' + \eta f'' - f = 0 \quad \text{and} \quad f' = \frac{s'}{\eta} \rightarrow f'' = \frac{s''}{\eta} - \frac{s}{\eta^2} \rightarrow f''' = \frac{s'''}{\eta} - \frac{2s''}{\eta^3} + \frac{2s'}{\eta^4}$$

$$f = \frac{s}{\eta} \rightarrow f' = \frac{s'}{\eta} - \frac{s}{\eta^2} \rightarrow f'' = \frac{s''}{\eta} - \frac{s}{\eta^3} \rightarrow f''' = \frac{s'''}{\eta} - \frac{s}{\eta^4} - \frac{s}{\eta^5}$$

$$\eta s''' - \frac{2s''}{\eta} + \frac{2s'}{\eta^3} + \cancel{\frac{s}{\eta^4}} - \cancel{\frac{s}{\eta^5}} + \frac{1}{2} \eta^2 (s'' - \frac{s}{\eta} + \cancel{\frac{s}{\eta^2}}) = 0$$

$$\eta s''' - s'' + \frac{1}{2} \eta^2 s'' = 0 \quad \text{and} \quad \ln s' = \ln s - \frac{1}{4} \eta^2 + \ln C$$

$$\frac{ds''}{s''} = \frac{1 - \frac{1}{2} \eta^2 dy}{\eta} \ln s' =$$

$$s'' = C \eta e^{-\frac{1}{4} \eta^2}$$

$$s' = C' e^{-\frac{1}{4} \eta^2} + D$$

$$f = \frac{C' e^{-\frac{1}{4} \eta^2} + D}{\eta}$$

$$V_D = \frac{P}{\sqrt{Dt}} \frac{\sqrt{Dt}}{n} \left[ C' e^{-\frac{n^2}{4Dt}} + D \right]$$

$$V_D = \frac{P}{n} \left[ D + C' e^{-\frac{n^2}{4Dt}} \right] \quad V_D \sim \frac{P}{2\pi n} \text{ for large } n$$

$$V_D = \frac{P}{n} \left[ D + C' e^{-\frac{n^2}{4Dt}} \right] \quad V_D = 0 \text{ at } n=0 \quad C' = -D$$

$$\Rightarrow D = \frac{1}{2\pi} \quad V_D = \frac{P}{2\pi n} \left[ 1 - e^{-\frac{n^2}{4Dt}} \right]$$

$$V_D = \frac{P}{2\pi n} \left[ 1 - e^{-\frac{n^2}{4Dt}} \right]$$