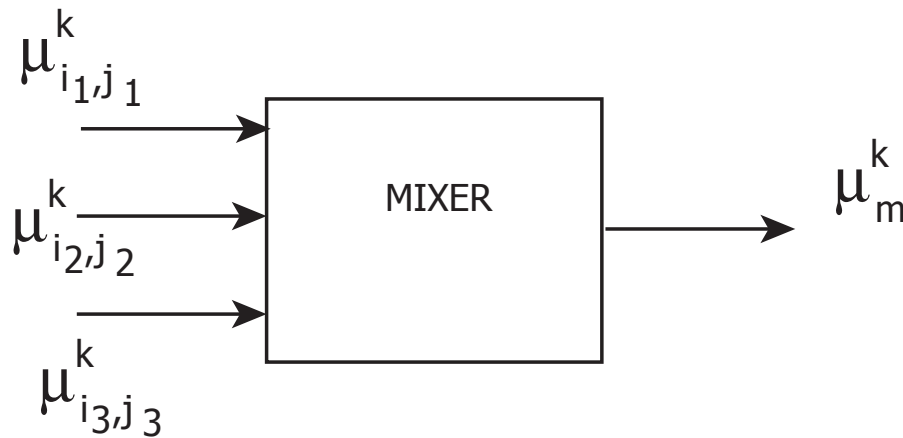


# Mixer, Splitter, and Reactor

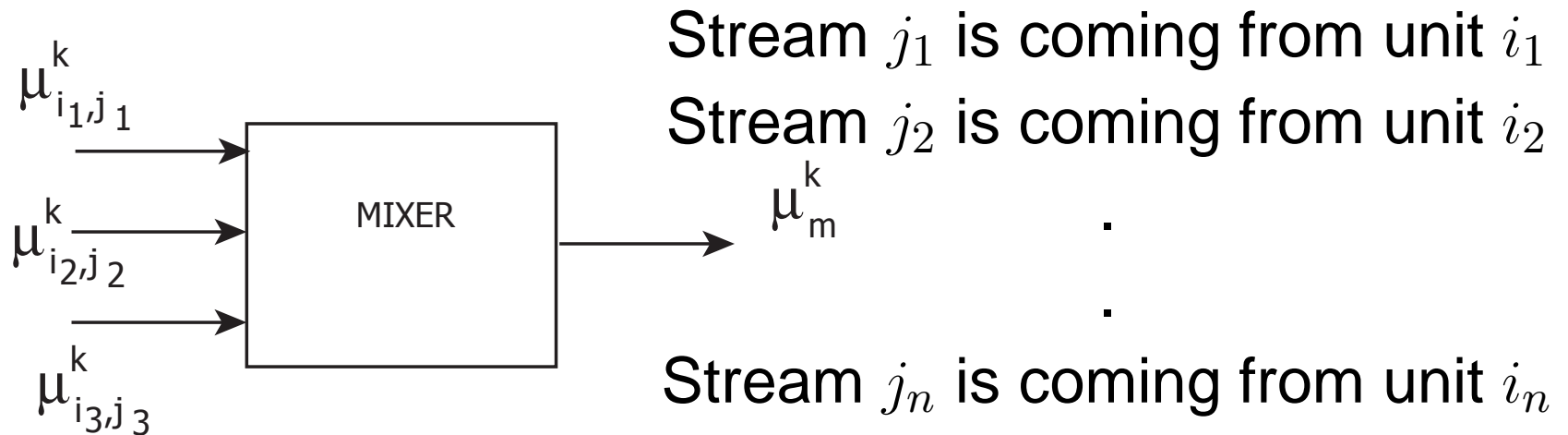
# Process Model: Mixer

Consider a mixer that is mixing  $n$  streams, each of which has  $k$  components.



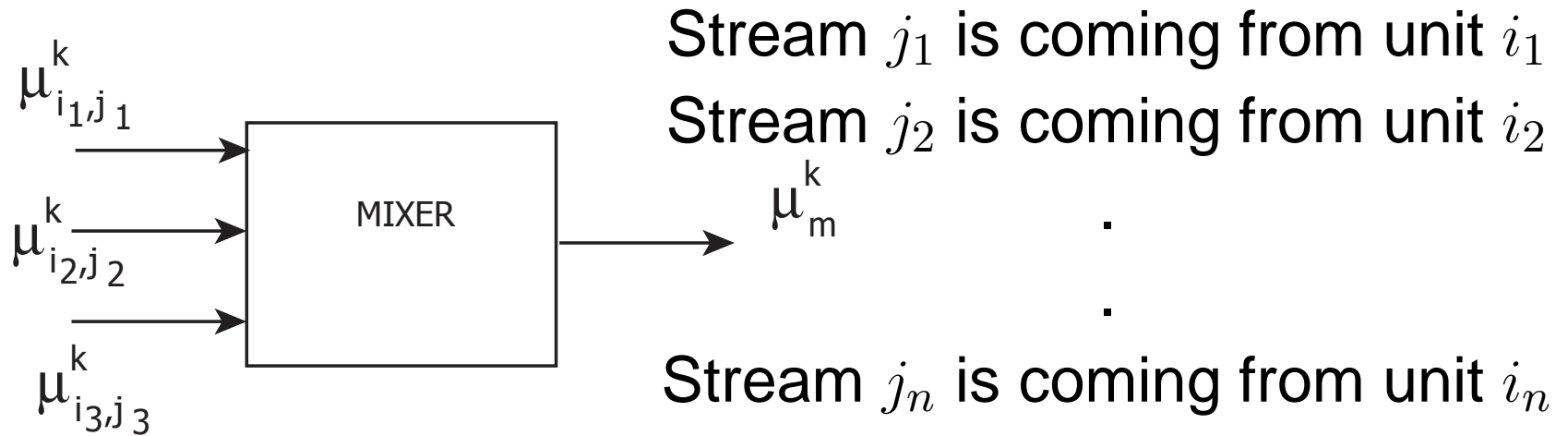
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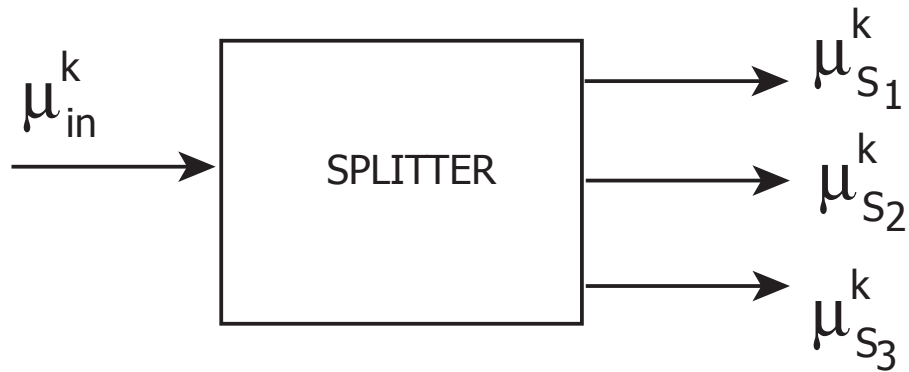
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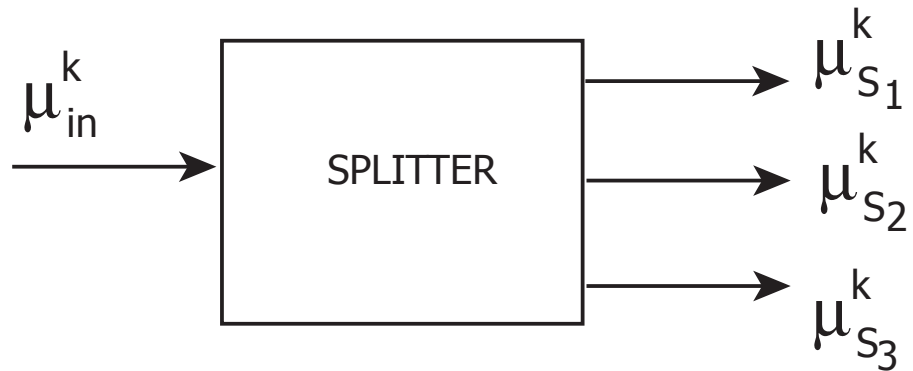
Then, the mixer balance for **component**  $k$  is given by:

$$\mu_m^k = \mu_{i_1, j_1}^k + \mu_{i_2, j_2}^k + \dots + \mu_{i_n, j_n}^k$$

# Process Model: Splitter



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$$\mu_{S_1}^k = \xi_1 \mu_{in}^k$$

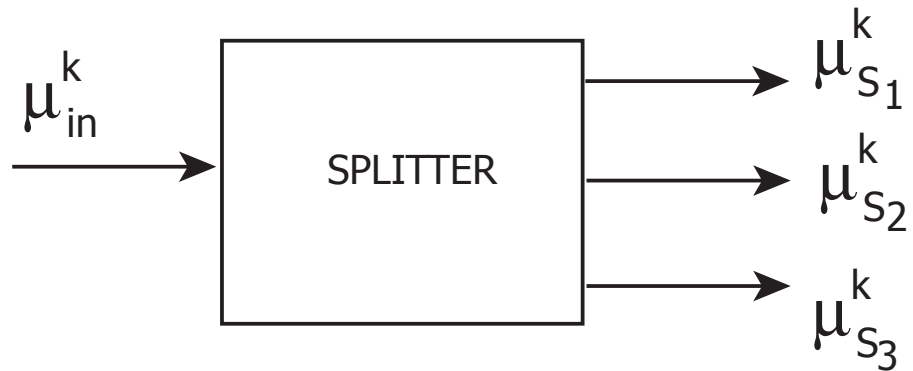
$$\mu_{S_2}^k = \xi_2 \mu_{in}^k$$

.

.

$$\mu_{S_{n-1}}^k = \xi_{n-1} \mu_{in}^k$$

# Process Model: Splitter



$$\mu_{S_1}^k = \xi_1 \mu_{in}^k$$

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.

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$$\mu_{S_{n-1}}^k = \xi_{n-1} \mu_{in}^k$$

$$\mu_{S_n}^k = [1 - (\xi_1 + \xi_2 + \dots + \xi_{n-1})] \mu_{in}^k$$

# Reactor

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- Specific Kinetic Model
- Equilibrium-based Reactor Model
- Stoichiometric Reactor Model

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- The reaction kinetics are typically determined via **laboratory experiments**.
- The **type** of reactor is taken into consideration in the model.

For instance, in a CSTR, the reactor model may be written as:

$$F.C - F.C_0 = V.r(C, T)$$

where  $r$  is the reaction rate



# Equilibrium-based Reactor Model

# Equilibrium-based Reactor Model

The equilibrium constant  $K$  is related to the free energy  $\Delta G$  and temperature  $T$  as follows:

$$K = \exp\left(-\frac{\Delta G}{RT}\right)$$

# Stoichiometric Reactor Model

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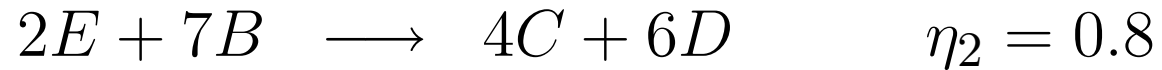
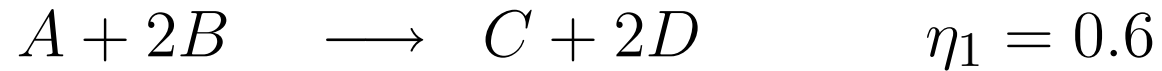
- The extent of reaction,  $\eta$ , for each reaction is **specified** by the user.
- The reaction stoichiometry is used to determine the **molar flowrate** of each species at steady state.

# Stoichiometric Reactor Model

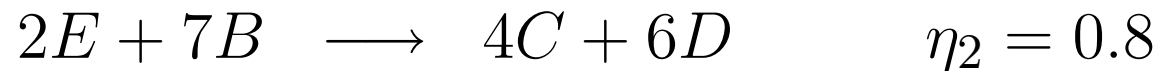
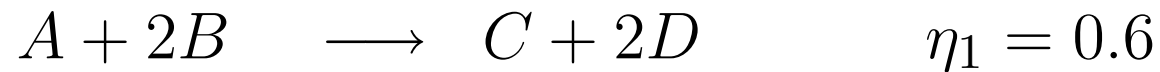
- The extent of reaction,  $\eta$ , for each reaction is **specified** by the user.
- The reaction stoichiometry is used to determine the **molar flowrate** of each species at steady state.
- The molar flow rates can be used to determine **reactor size**.

# Stoichiometric Reactor Calculations

# Stoichiometric Reactor Calculations



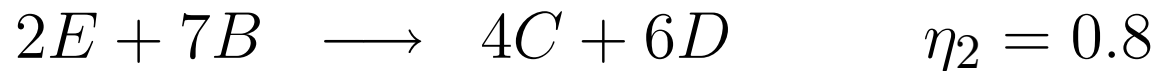
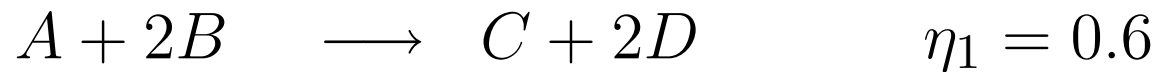
# Stoichiometric Reactor Calculations



It is given that  $A$  is the **limiting** reactant for the first reaction (with 60% conversion) and  $E$  is the limiting reactant for the second reaction (with 80% conversion).



# Stoichiometric Reactor Calculations



It is given that  $A$  is the **limiting** reactant for the first reaction (with 60% conversion) and  $E$  is the limiting reactant for the second reaction (with 80% conversion).

If the molar flowrate of each species coming **into** the reactor is known, compute the molar flowrate of each species going **out** of the reactor.

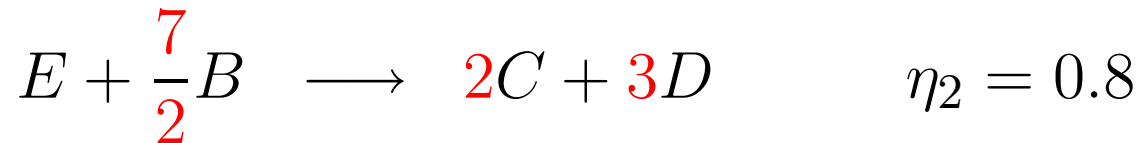
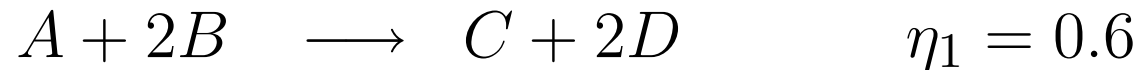
# Stoichiometric Reactor Calculations

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Step 1: Normalize all reactions w.r.t. limiting reactants.

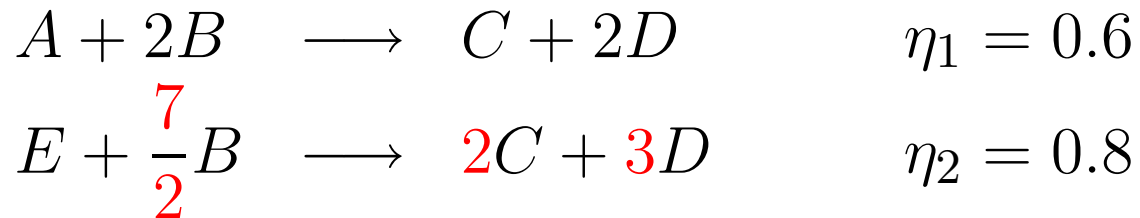
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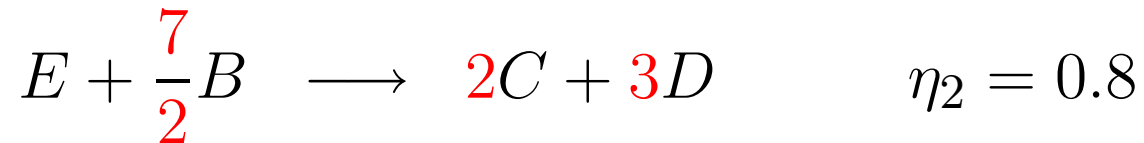
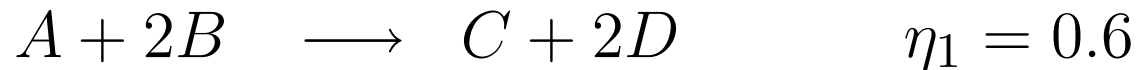


Step 2: Generate stoichiometric table using the convention:

Reactants have **negative** sign, inerts are **zero** and products have **positive** sign.

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Step 2: Generate stoichiometric table using the convention:

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r	A	B	E	C	D
1	-1	-2	0	1	2
2	0	-7/2	-1	2	3

# Stoichiometric Reactor Calculations

Step 3: Write down the mass balance for the **limiting** reactants.

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$$\begin{aligned}\mu_R^A &= \mu_{in}^A - 0.6\mu_{in}^A = 0.4\mu_{in}^A \\ \mu_R^E &= \mu_{in}^E - 0.8\mu_{in}^E = 0.2\mu_{in}^E\end{aligned}$$

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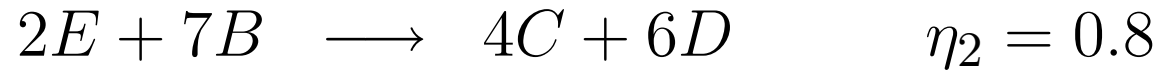
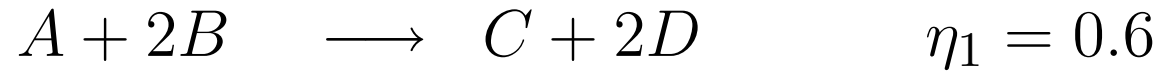
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$$\begin{aligned}\mu_R^B &= \mu_{in}^B - 2(0.6\mu_{in}^A) - \frac{7}{2}(0.8\mu_{in}^E) \\ \mu_R^C &= \mu_{in}^C + 0.6\mu_{in}^A + 2(0.8\mu_{in}^E) \\ \mu_R^D &= \mu_{in}^D + 2(0.6\mu_{in}^A) + 3(0.8\mu_{in}^E)\end{aligned}$$

Note that in Steps 3 and 4, all equations are linear.

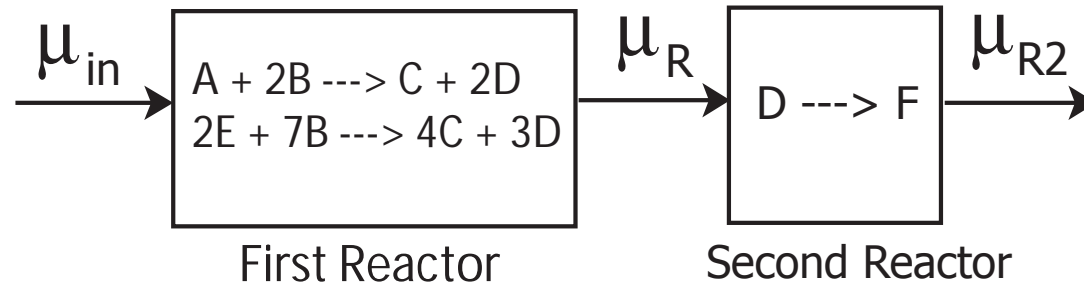
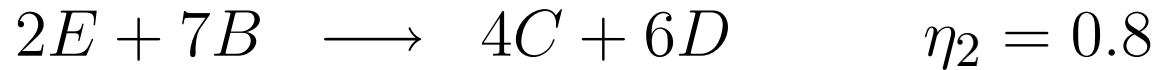
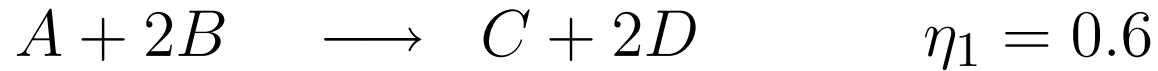
# Series reactions

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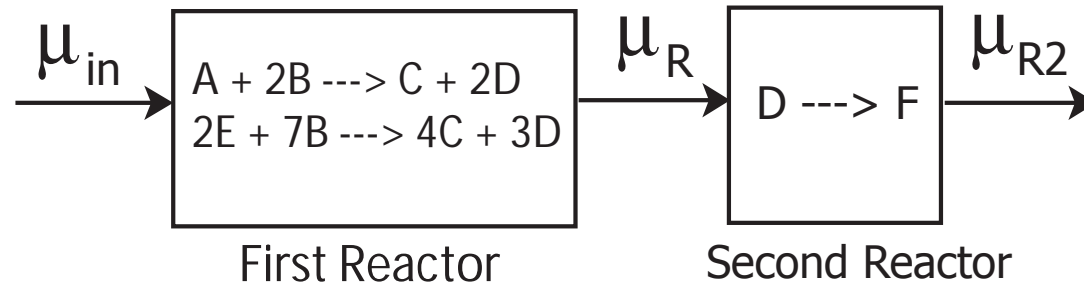
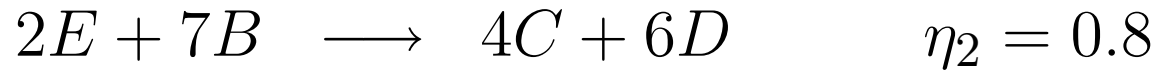
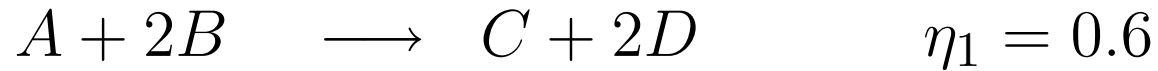




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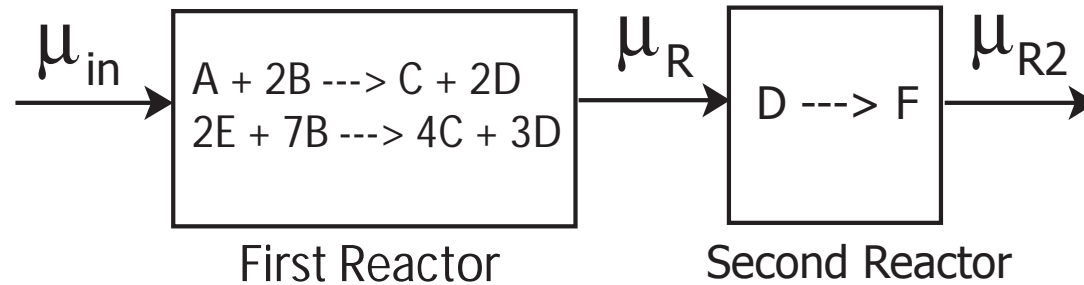
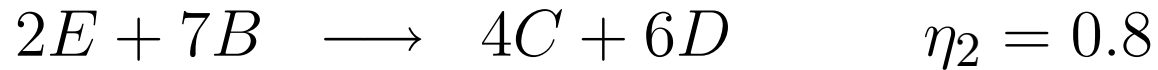
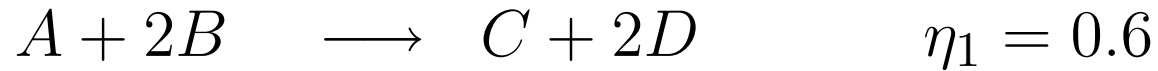


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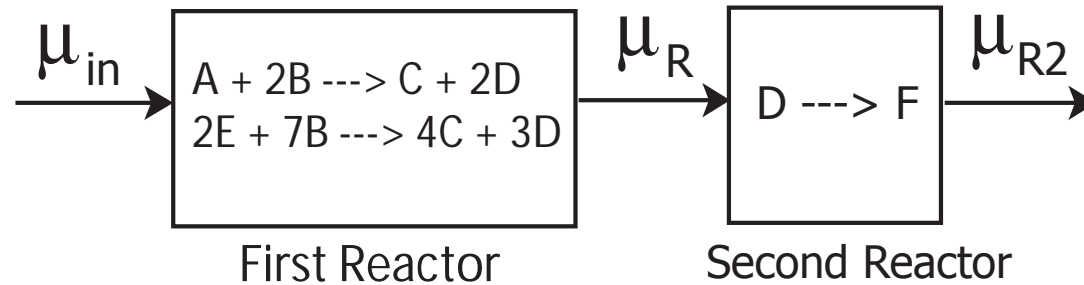
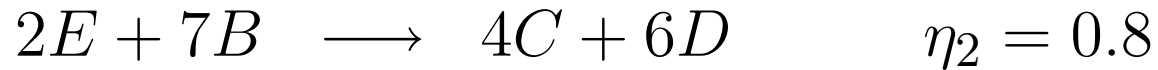
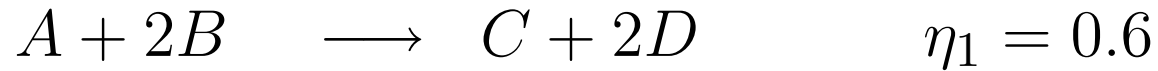
**Balances for first reactor:**

# Series reactions



**Balances for first reactor:** Same as before

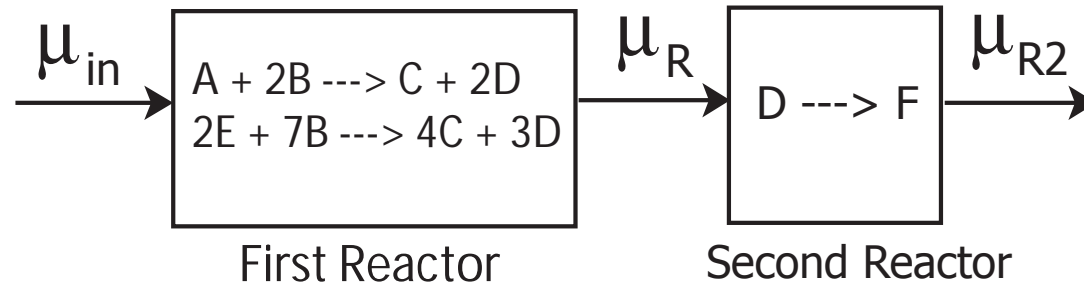
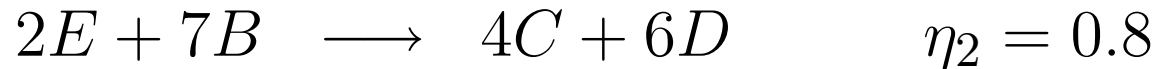
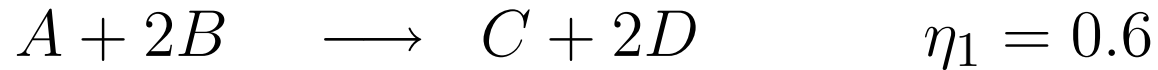
# Series reactions



**Balances for first reactor:** Same as before

**Balances for second reactor:**

# Series reactions



**Balances for first reactor:** Same as before

**Balances for second reactor:**

$$\begin{aligned} \mu_{R2}^D &= \mu_R^D - 0.7\mu_R^D = 0.3\mu_R^D \\ \mu_{R2}^F &= \mu_R^F + 0.7\mu_R^D \end{aligned}$$