

Energy Balances

One man's magic is another man's engineering.

Lazarus Long

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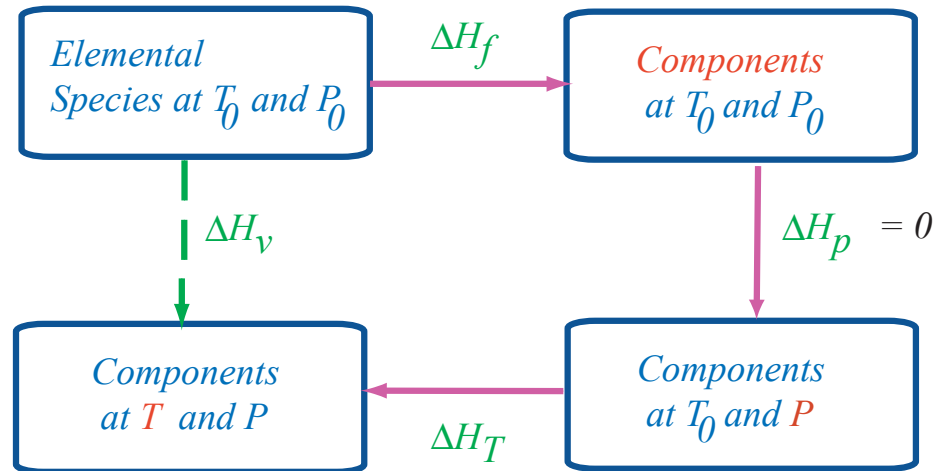
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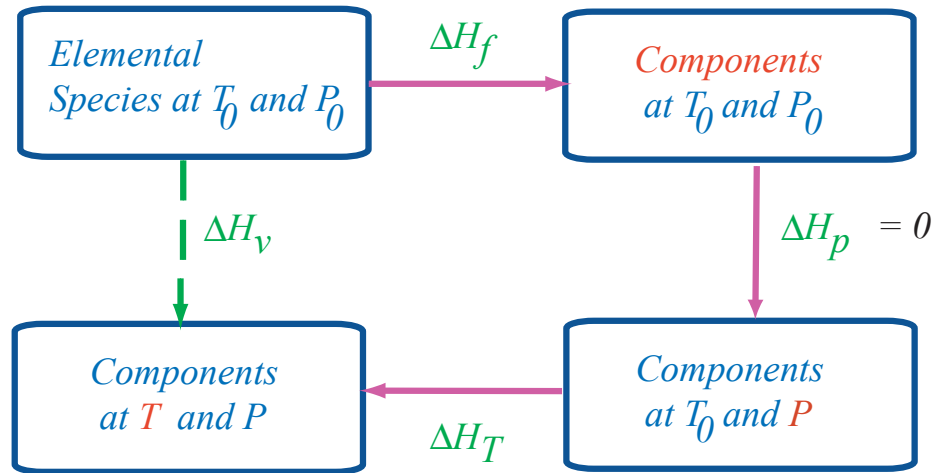
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 3. Standard enthalpy reference ($\Delta H = 0$) is at $P_0 = 1 \text{ atm}$, $T_0 = 298 \text{ K}$ and elemental species.

Enthalpies of Vapor Streams

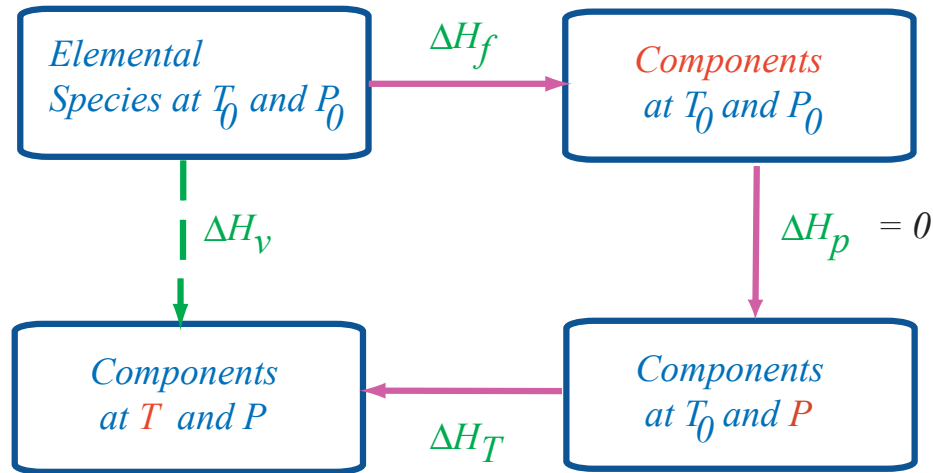


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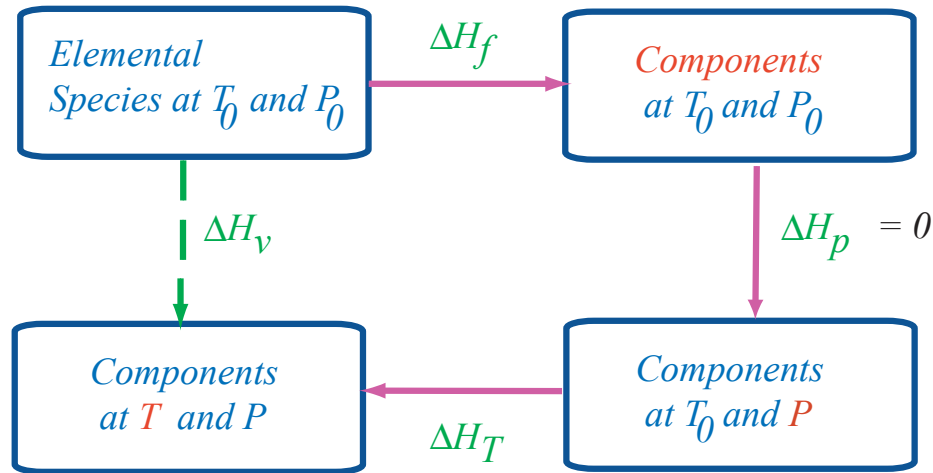
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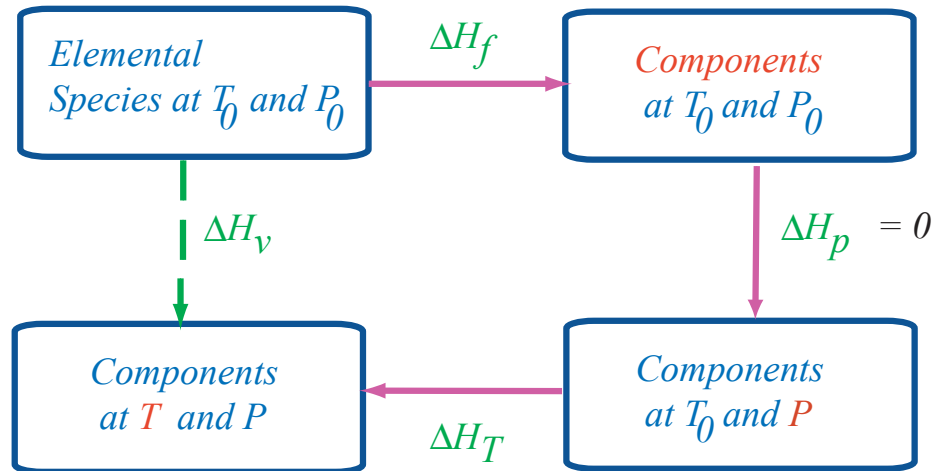
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$$\Delta H_f = y_1 H_{f,1}(T_0) + \dots + y_n H_{f,n}(T_0)$$

where $H_{f,k}(T_0)$ is the heat of formation of component k at temperature T_0 .

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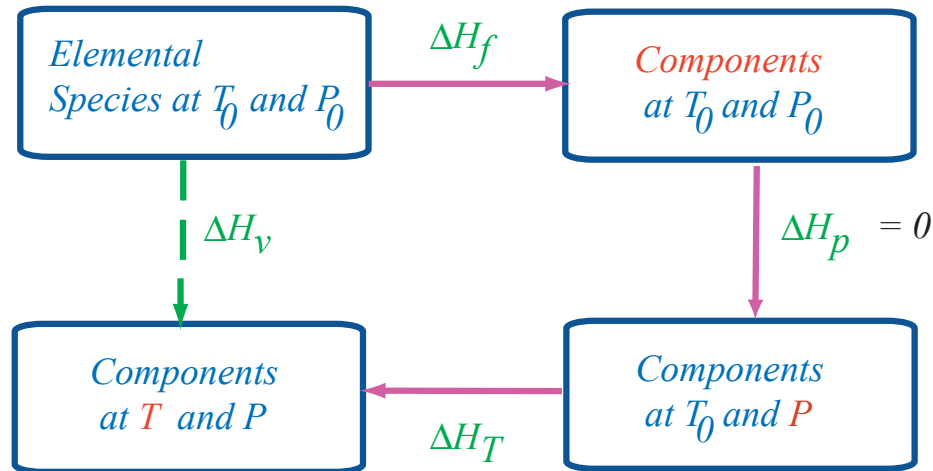
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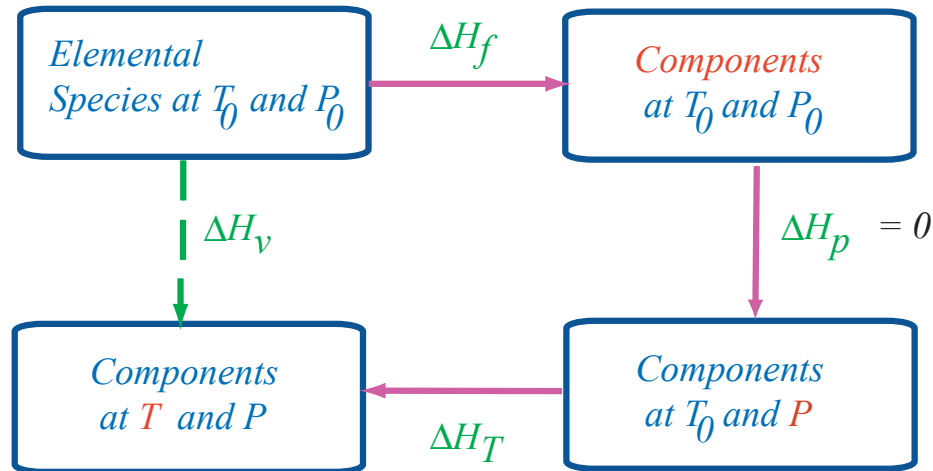
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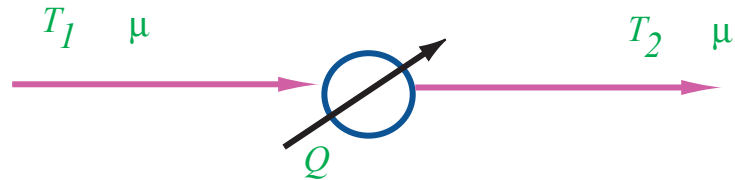
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Heat Exchanger Calculation

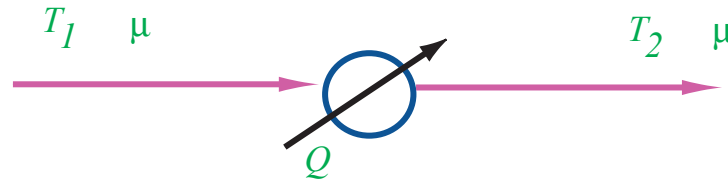
Consider a heat exchanger with no phase change.



There is temperature change but no composition change.

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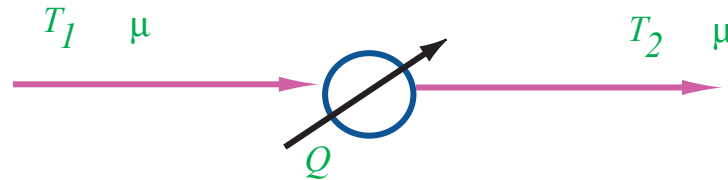


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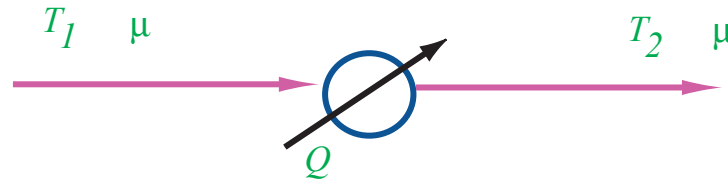
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Since composition does not change, ΔH_f at T_0 is the same on both sides of heat balance and thus cancels out.

$$(\cancel{\mu\Delta H_f})_{in} + (\mu\Delta H_T)_{in} + Q = (\cancel{\mu\Delta H_f})_{in} + (\mu\Delta H_T)_{out}$$

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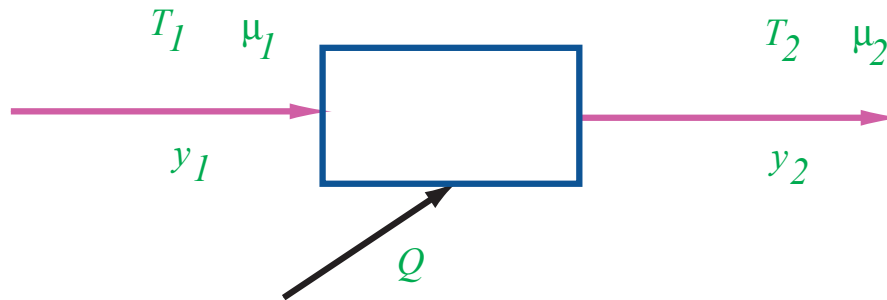
$$(\cancel{\mu\Delta H_f})_{in} + (\mu\Delta H_T)_{in} + Q = (\cancel{\mu\Delta H_f})_{in} + (\mu\Delta H_T)_{out}$$

This implies:

$$Q = \mu \left(y_1 \int_{T_1}^{T_2} c_{p,1}^0 dT + \dots + y_n \int_{T_1}^{T_2} c_{p,n}^0 dT \right)$$

Reactor Calculation

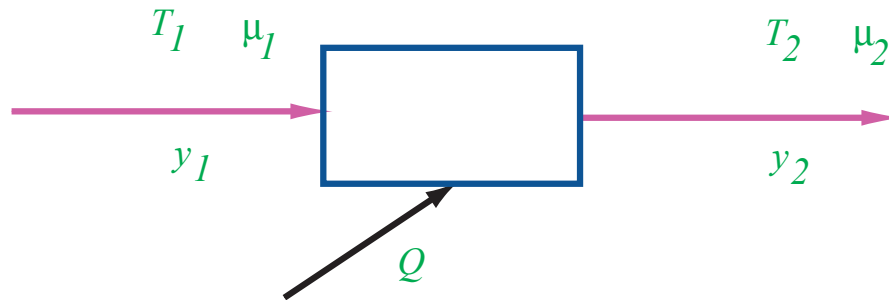
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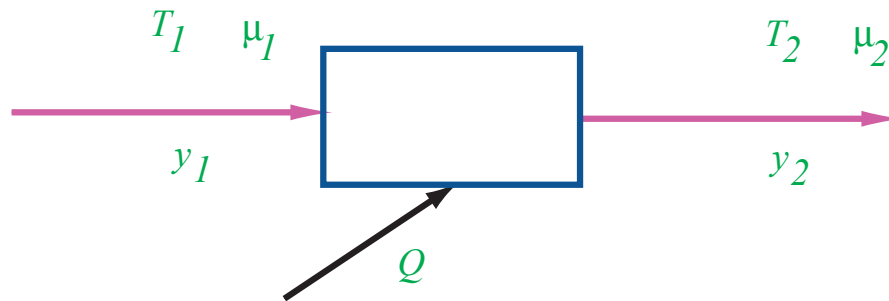


There is temperature change as well as composition change. At steady state:

$$[\mu_1 \Delta H(T_1, y_1)]_{in} + Q_R = [\mu_2 \Delta H(T_2, y_2)]_{out}$$

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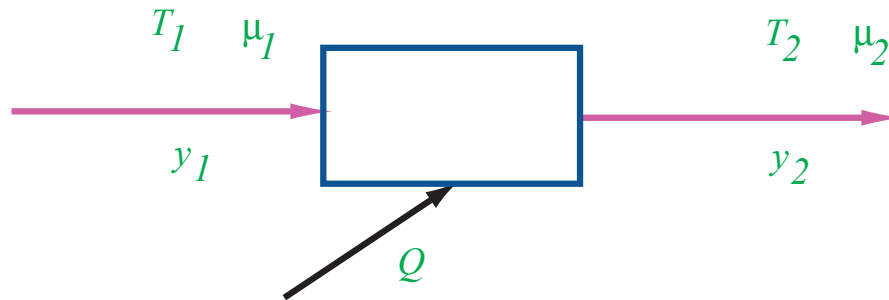
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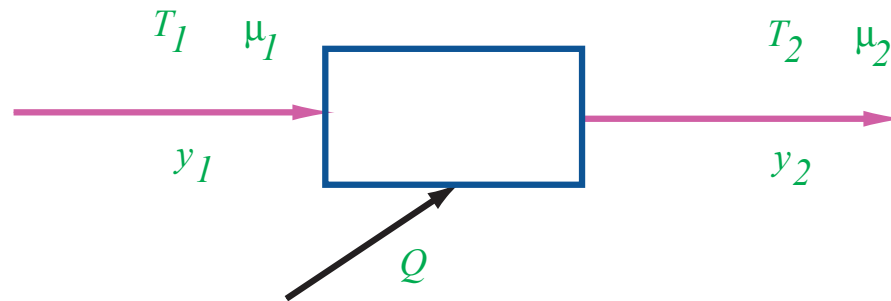
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$Q_R > 0 \implies$ reaction is **endothermic**.

$Q_R < 0 \implies$ reaction is **exothermic**.

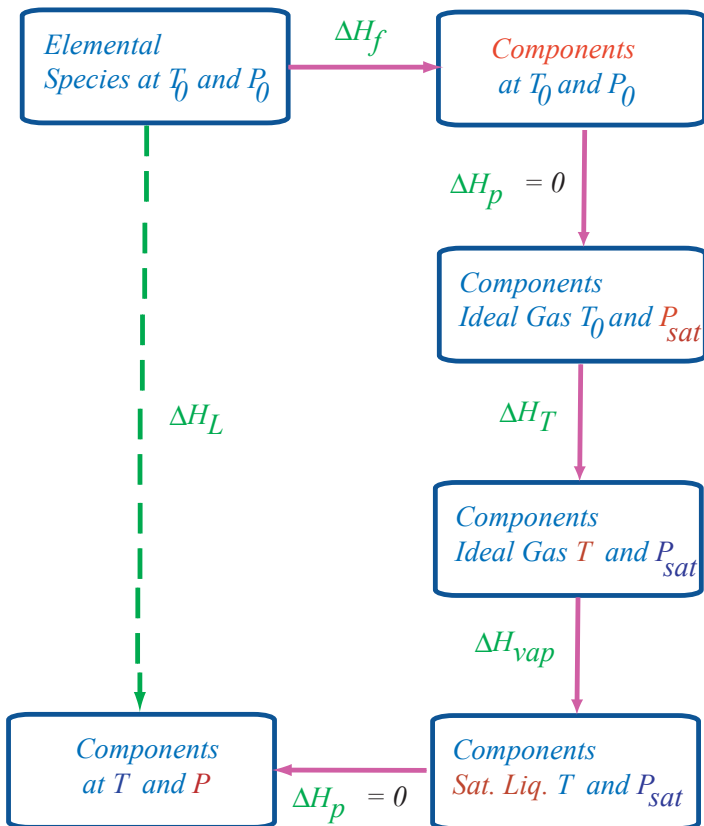
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Enthalpies of liquid mixtures are evaluated directly from the ideal **vapor** enthalpy and **subtracting** the **heat of vaporization** at saturation conditions.

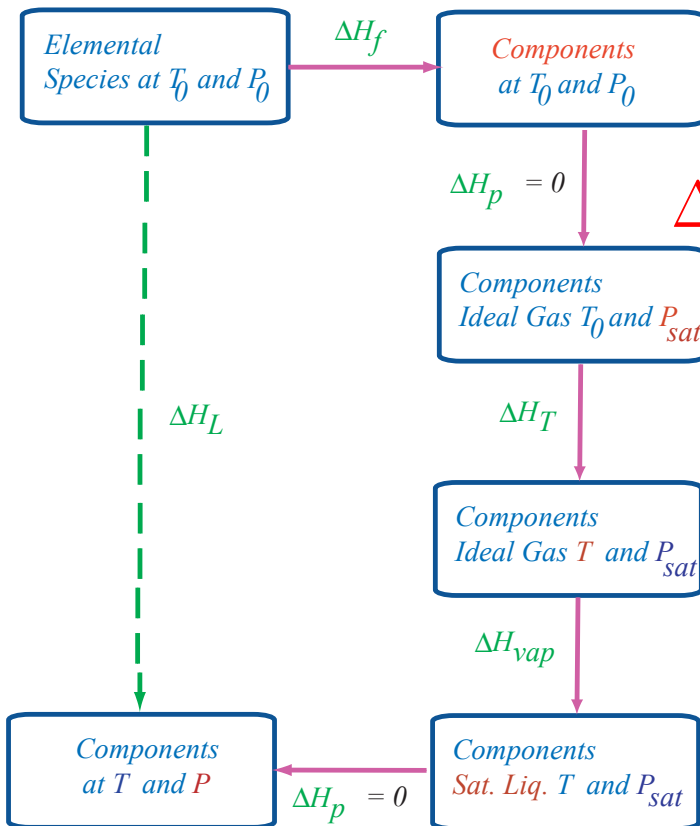
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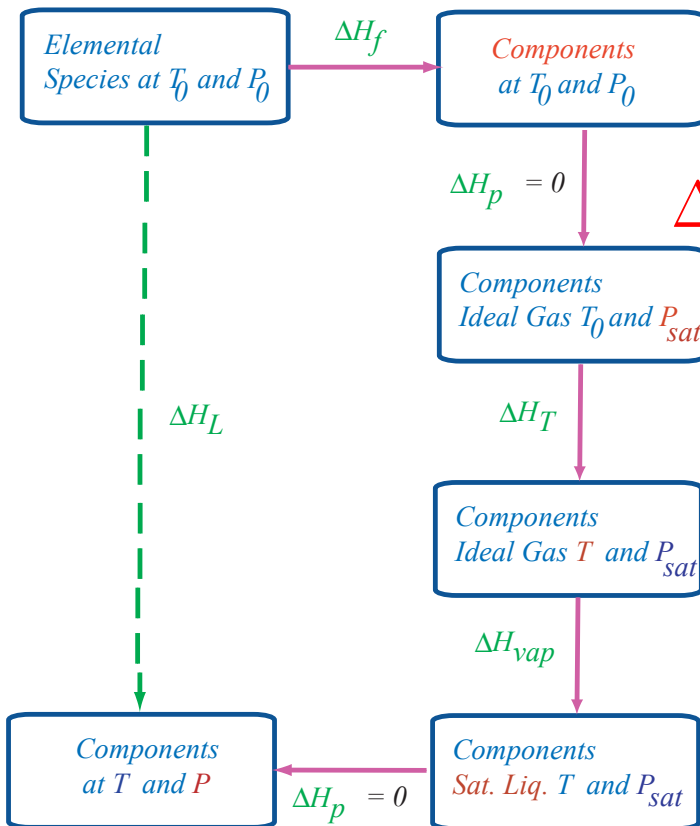
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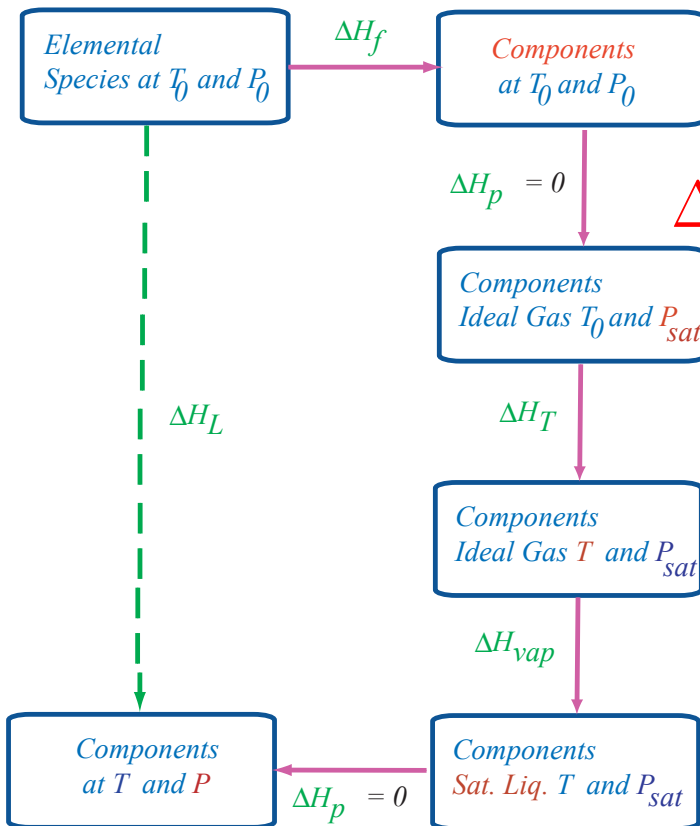


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$$\Delta H_{vap}^k(T) = \Delta H_{vap}^k(T_b) \left[\frac{(T_c^k - T)}{(T_c^k - T_b)} \right]^{0.38}$$

T_c^k : critical temperature

T_b^k : boiling point at 1 atm

$\Delta H_{vap}^k(T_b)$ heat of vaporization at T_b^k

Liquid Mixtures and Two Phase Mixtures

- The specific stream enthalpy for liquid **mixtures** is estimated as a **weighted sum** of respective mole fractions.

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- For a **vapor-liquid mixture** with vapor fraction ϕ , the stream enthalpy is given by the weighted sum of the liquid and vapor enthalpies.

$$\Delta H_L(T, x) = \phi \Delta H_V(T, y) + (1 - \phi) \Delta H_L(T, x)$$

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T_V, P_V specified

Isothermal flash

$V/F = 0, P_L$ specified

Bubble point temperature

$V/F = 1, P_V$ specified

Dew point temperature

T_L specified, $V/F = 0$

Bubble point pressure

T_V specified, $V/F = 1$

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Adiabatic flash

Q, P_V specified

Nonadiabatic flash

$V/F, P_V$ specified

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$Q = 0, P_V$ specified	Adiabatic flash
Q, P_V specified	Nonadiabatic flash
$V/F, P_V$ specified	Percent vaporization flash

We did **not** consider the flash calculations that involved energy balance. We will consider the adiabatic flash now.

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Scenario: Heat is added to a liquid mixture stream due to which part of it vaporizes. What is the flash temperature and what are the compositions of the liquid and vapor streams if the pressure is specified?

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- If $\Delta H_{dew} \geq \Delta H_{spec} \geq \Delta H_{bub}$, guess ξ_n (or ϕ).

- Perform a flash calculation with ξ_n (or ϕ) and P specified to obtain y_k , x_k and T .
Calculate $\Delta H(T) = \phi\Delta H_v + (1 - \phi)\Delta H_L$

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Calculate $\Delta H(T) = \phi\Delta H_v + (1 - \phi)\Delta H_L$
- If $f = \Delta H_{spec} - \Delta H(T) = 0$ **STOP**. Otherwise, if $f > 0$ reguess a **higher** ξ_n (or ϕ), else guess a lower ξ_n (or ϕ) and go back to previous step.

Illustrative Example

Consider a 50-50 liquid mixture of benzene and toluene flowing at 100 gmol/s at 300 K and 1 bar . If heat is added to this stream at the rate of 860.42 kcal/s , what is the **temperature** of the mixture.

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$$860.42 - 847.50 = 12.868 \text{ kcal/s}$$

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Compute $\alpha_{B/T} = 2.453$ at $T = 370 \text{ K}$.
 - Guess ξ_T and solve for ξ_B , ϕ and T from:

$$\xi_B = \frac{\alpha_{B/T}\xi_T}{1 + (\alpha_{B/T} - 1)\xi_T}$$

$$\phi = \frac{50(\xi_B + \xi_T)}{100}$$

$$P_T^0(T) = \frac{P}{\bar{\alpha}}$$

- With this information, calculate:

$$\Delta H(T) = \phi \Delta H_V(T) + (1 - \phi) \Delta H_L(T)$$

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0.585	0.776	369.5	0.680	12.993

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0.570	0.765	369.4	0.667	4.895
0.585	0.776	369.5	0.680	12.993

Thus, the stream is 68% vaporized at a temperature of 369.5 K.