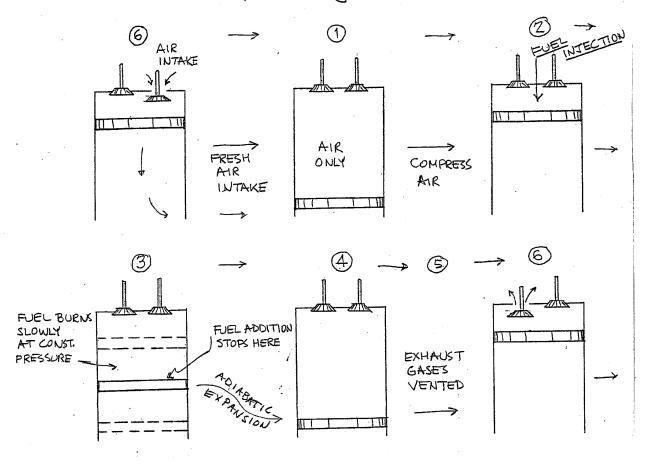
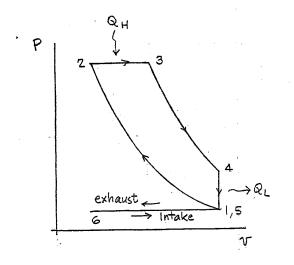
## Diesel Engine Cycle

The diesel engine is a four-stroke internal combustion engine. Combustion of the air-fuel mixture occurs through compression ignition.

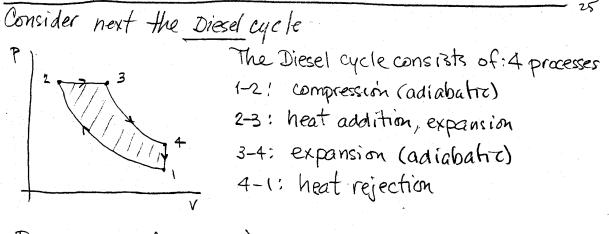


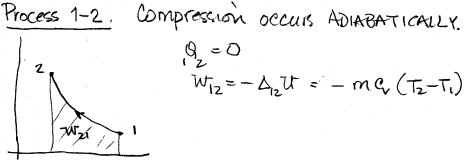


 $r_v = \frac{V_1}{V_2}$  volumetric compression ratio

rc= V3 cutoff ratio

DIESEL Cycle





 $\begin{aligned} & \theta_z = 0 \\ & W_{1z} = -\Delta_{1z} U = -m C_v (T_z - T_i) \end{aligned}$ Process 2-31. Heat addition at anstaut pressure  $W_{23} = \int p dV = p_2 \left( dV = p_2 \left( V_3 - V_2 \right) \right)$  $= mR(T_3 - T_2) \qquad \text{Note: } p_2 = p_3 = const.$ P AT= Q2 -W23  $= c_0(T_a - T_b)$ Proper 3-4 ADIABATY PRODUCION

$$\frac{112253}{3} = 0$$

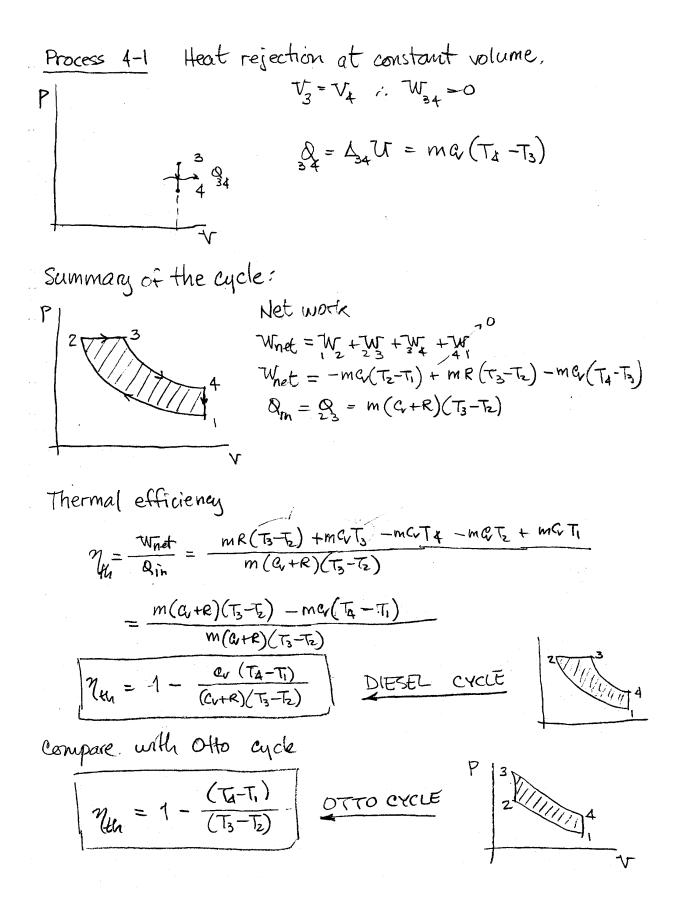
$$\frac{3}{34} = 0$$

$$\frac{3}{34} = -434$$

$$W_{1} = -MGr(T_{4} - T_{3})$$

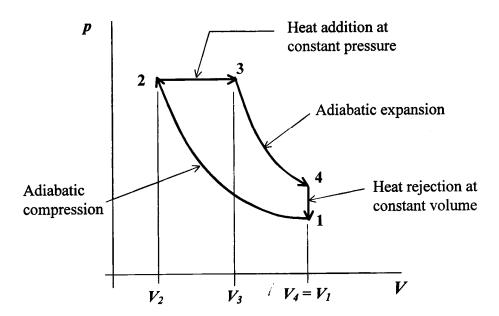
$$W_{1} = -MGr(T_{4} - T_{3})$$

$$W_{1} = -MGr(T_{4} - T_{3})$$



Consider and ideal Diesel engine cycle in which the pressure and temperature at the beginning of the adiabatic compression process are 100 kPa and 27°C, the volumetric compression ratio is 18 ( $r_v = v_1/v_2 = 18$ ), and the cutoff ratio for the cycle is 2 ( $r_c = v_3/v_2 = 2$ ). Analyze each of the four processes in this cycle for work and heat transfer, state variables, and determine the thermal efficiency. Conduct your calculations assuming constant specific heat capacity as given below.

Assume the working fluid is air with  $c_v = 0.718 \text{ kJ/kg-K}$ , cp = 1.005 kJ/kg-K, k = 1.4 R = 0.287 kJ/kg K



State	p (kPa)	$v (m^3/kg)$	T (°C)	Process	∆u (kJ/kg)	<i>q</i> (kJ/kg)	w (kJ/kg)
1	100		27	1-2		· · · · · · · · · · · · · · · ·	
2				2-3			
3	· · · · · · · · · · · · · · · · · · ·		· · ·	3-4		····	
4				4-1			
				TOTAL			

Cycle efficiency:

## **Diesel Cycle Example calculation**

Initial conditions are given in terms of the initial pressure, temperature, the volume compression ratio, v1/v2 = 18, and the cutoff ratio, v3/v2 = 2.

Units setup:  $kJ := 10^3 \cdot J$   $kPa := 10^3 \cdot Pa$ 

The system is air with the following properties:  $R := 0.287 \frac{J}{gm \cdot K}$   $c_v := 0.718 \frac{J}{gm \cdot K}$  k := 1.40

Given information 
$$p_1 := 100 \text{ kPa}$$
  $T_1 := 300 \text{ K}$   $r_v := \frac{v_1}{v_2}$   $r_v := 18$   $r_c := \frac{v_3}{v_2}$   $r_c := 2$ 

Calculation of v1 from the ideal gas relationship pv = RT.  $v_1 := \frac{R \cdot T_1}{p_1}$   $v_1 = 0.861 \frac{m^3}{kg}$ 

**Process 1 - 2:** Adiabatic compression.  $q_{12} := 0 \cdot \frac{kJ}{kg}$ 

$$v_2 := \frac{v_1}{r_v}$$
  $v_2 = 0.048 \frac{m^3}{kg}$   $p_2 := p_1 \cdot \left(\frac{v_1}{v_2}\right)^k$   $p_2 = 5.72 \times 10^6 Pa$   $T_2 := \frac{p_2 \cdot v_2}{R}$   $T_2 = 953.301 K$ 

Calculation of work 
$$w_{12} := \frac{p_2 \cdot v_2 - p_1 \cdot v_1}{1 - k}$$
  $w_{12} = -468.744 \frac{kJ}{kg}$ 

Calculation of internal energy change from the first law  $\Delta u_{12} := -w_{12}$   $\Delta u_{12} = 468.744 \frac{kJ}{kg}$ 

Note that work can be calculated directly from its integral expression  $w_{12} = \int_{v_1}^{v_2} p(v) dv$ 

where  $p(v) := p_1 \cdot \left(\frac{v_1}{v}\right)^k$   $w_{12} := \int_{v_1}^{v_2} p(v) \, dv$   $w_{12} = -468.744 \frac{kJ}{kg}$ 

**Process 2 - 3:** Heat addition at constant pressure:  $p_3 := p_2$   $p_3 = 5.72 \times 10^3 \text{ kPa}$ 

$$v_3 := r_c \cdot v_2$$
  $v_3 = 0.096 \frac{m^3}{kg}$ 

From the ideal gas law equation of state:  $T_3 := \frac{p_3 \cdot v_3}{R}$   $T_3 = 1.907 \times 10^3 \text{ K}$ Calculation of work  $w_{23} := p_2 \cdot (v_3 - v_2)$   $w_{23} = 273.598 \frac{kJ}{kg}$ Calculation of internal energy change  $\Delta u_{23} := c_v \cdot (T_3 - T_2)$   $\Delta u_{23} = 684.47 \frac{kJ}{kg}$ 

Calculation of heat transfer from the first law

$$q_{23} := \Delta u_{23} + w_{23}$$
  $q_{23} = 958.068 \frac{kJ}{kg}$ 

**Process 3 - 4:** Adiabatic expansion.  $q_{34} := 0 \cdot \frac{kJ}{kg}$ 

$$v_4 := v_1$$
  $p_4 := p_3 \cdot \left(\frac{v_3}{v_4}\right)^k$   $p_4 = 2.639 \times 10^5 \text{ Pa}$   $T_4 := \frac{p_4 \cdot v_4}{R}$   $T_4 = 791.705 \text{ K}$ 

 $\begin{array}{ll} \mbox{Calculation of the change in internal energy} & \Delta u_{34} \coloneqq c_v \cdot \left(T_4 - T_3\right) & \Delta u_{34} = -800.497 \frac{kJ}{kg} \\ \mbox{Calculation of work from the first law} & w_{34} \coloneqq -\Delta u_{34} & w_{34} = 800.497 \frac{kJ}{kg} \end{array}$ 

Process 4 - 1: Heat rejection at constant volume .  $w_{41} := 0 \cdot \frac{kJ}{k\sigma}$ 

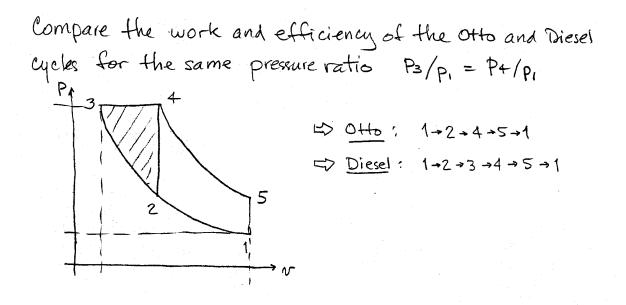
$$\mathbf{p}_4 \coloneqq \mathbf{p}_1 \cdot \left(\frac{\mathbf{T}_4}{\mathbf{T}_1}\right) \quad \mathbf{p}_4 = 263.902 \mathrm{kPa}$$

 $\begin{array}{ll} \mbox{Calculation of the change in internal energy} & \Delta u_{41} := c_v \cdot \left(T_1 - T_4\right) & \Delta u_{41} = -353.044 \frac{kJ}{kg} \\ \mbox{Calculation of the heat transfer from the first law} & q_{41} := \Delta u_{41} & q_{41} = -353.044 \frac{kJ}{kg} \end{array}$ 

Cycle summation:
$$q_{net} := q_{12} + q_{23} + q_{34} + q_{41}$$
 $q_{net} = 605.024 \frac{kJ}{kg}$  $w_{net} := w_{12} + w_{23} + w_{34} + w_{41}$  $w_{net} = 605.351 \frac{kJ}{kg}$ 

$$\Delta u_{net} := \Delta u_{12} + \Delta u_{23} + \Delta u_{34} + \Delta u_{41} \qquad \Delta u_{net} = -0.327 \frac{kJ}{kg}$$

Cycle efficiency: 
$$q_{in} := q_{23}$$
  $q_{in} = 958.068 \frac{kJ}{kg}$   
 $\eta := \frac{w_{net}}{q_{in}}$   $\eta = 0.632$ 



Comparison between Otto (gasoline) and Diesel engines

