

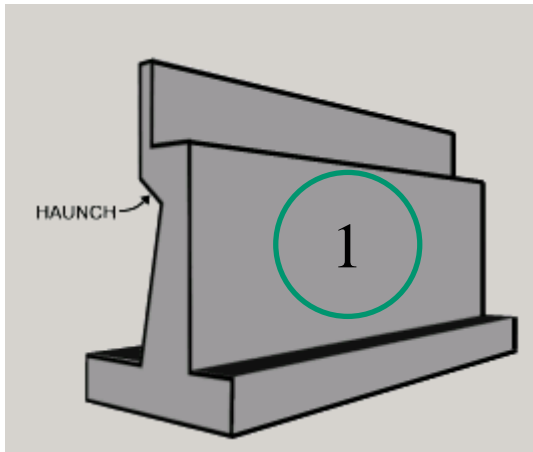
Mechanically Stabilized Earth (MSE) Wall

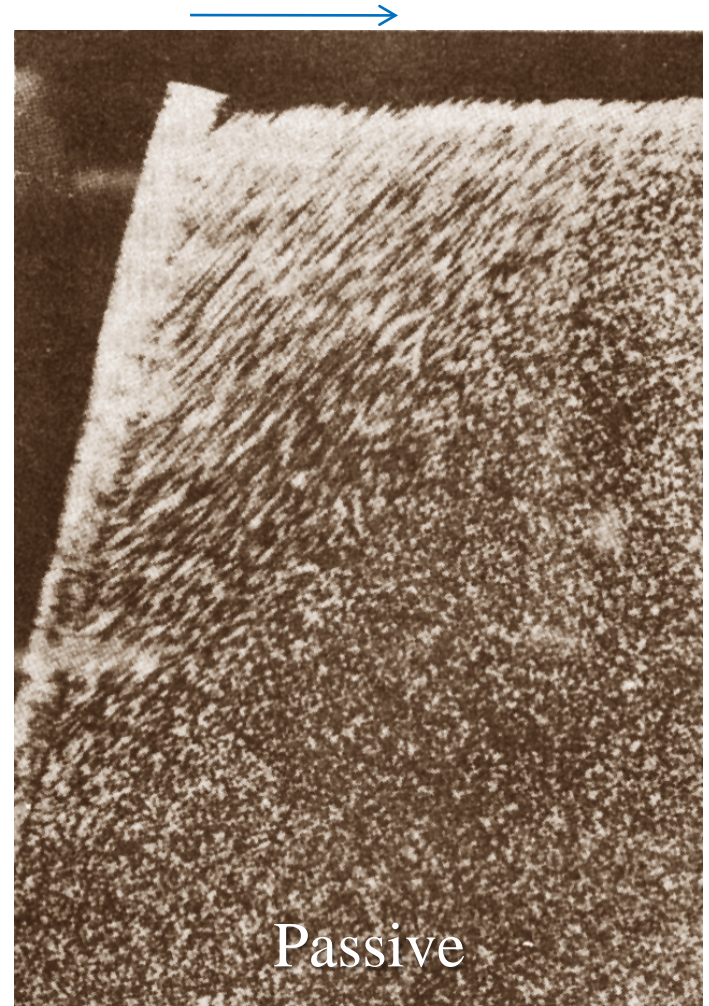
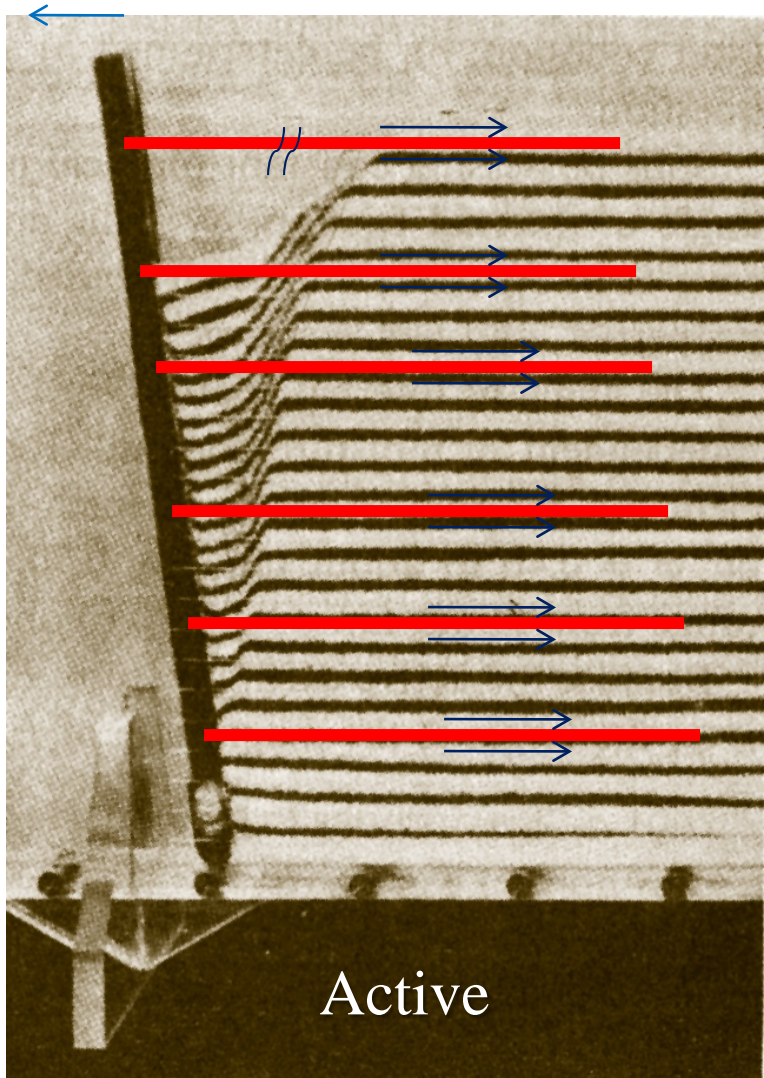
Geotechnical Design

CEG 4801

Kamal Tawfiq, Ph.D., P.E.

Choices for Bridge Abutments

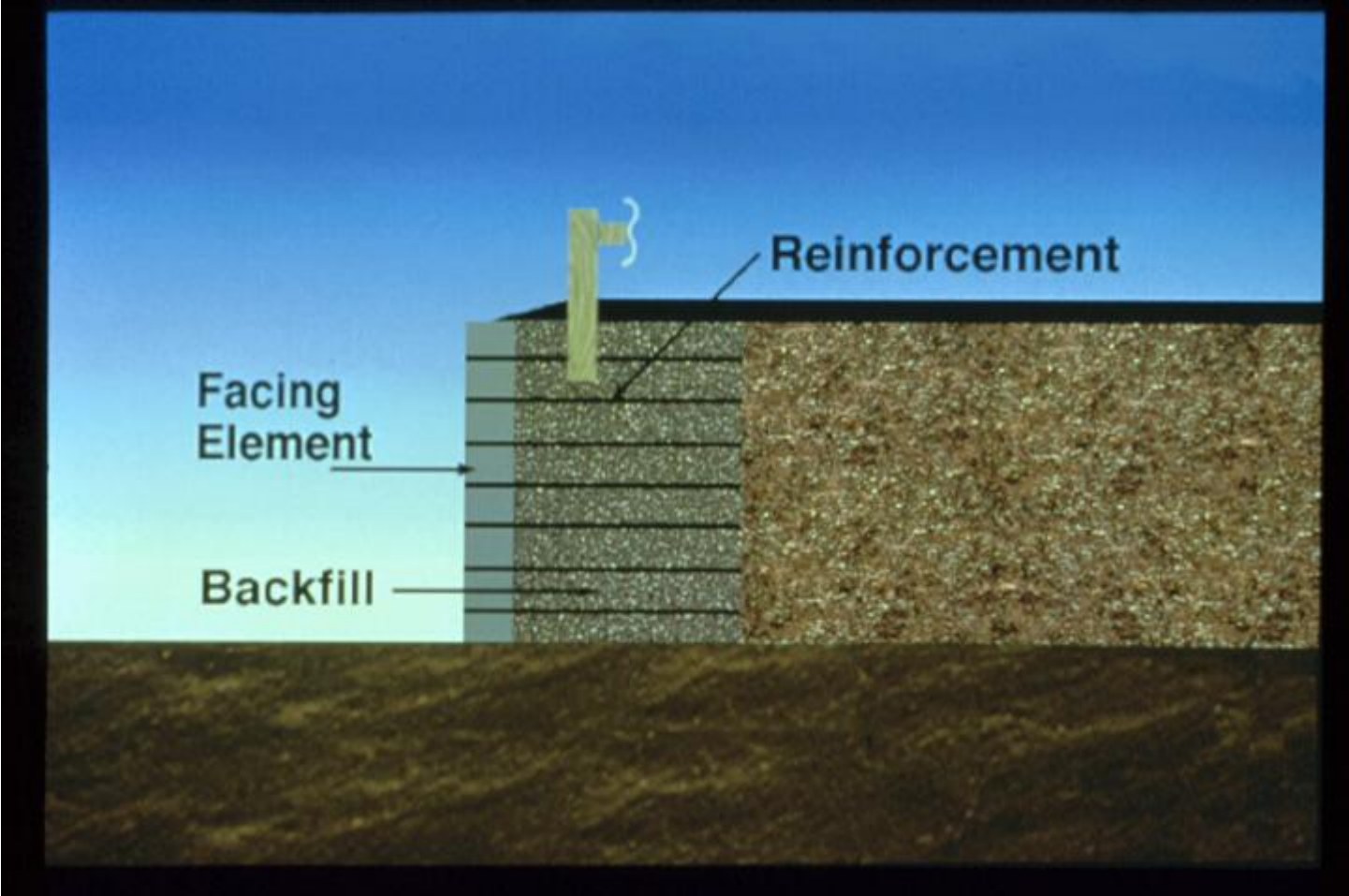




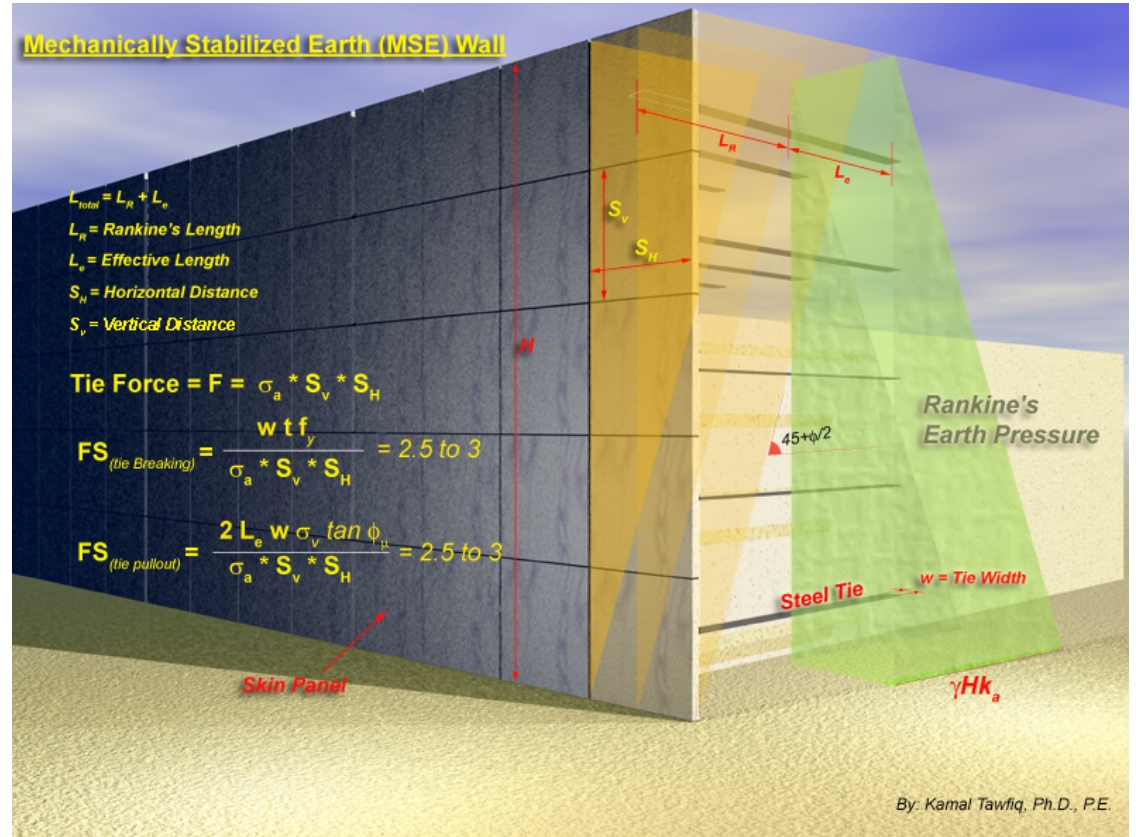
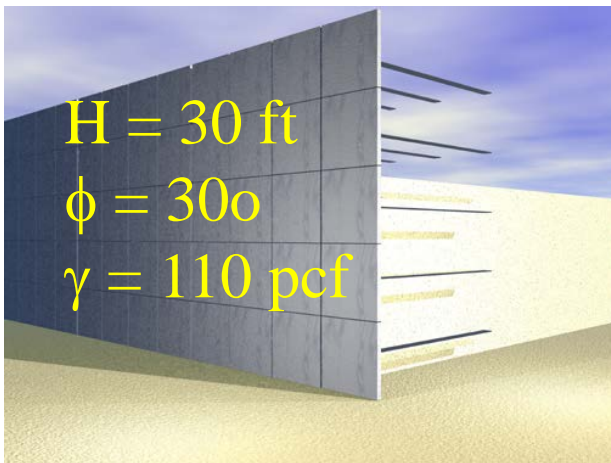
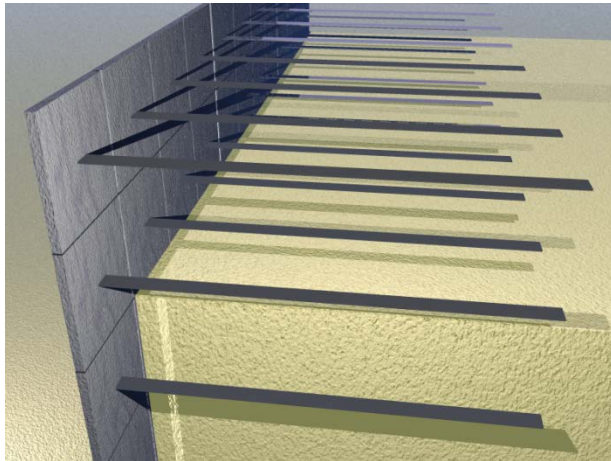
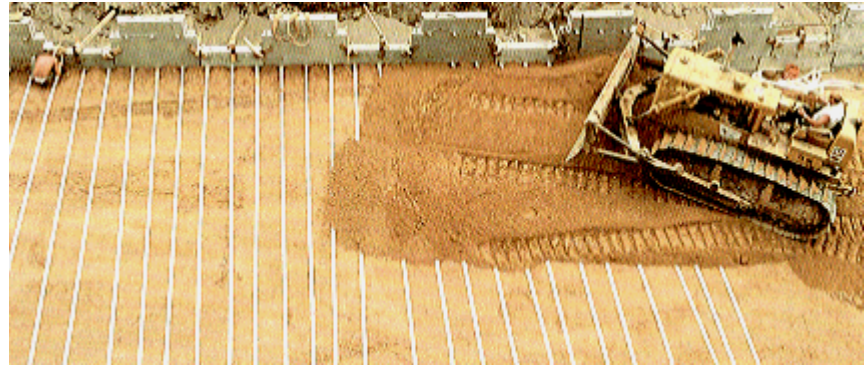
Earth Pressure Behind Retaining Wall

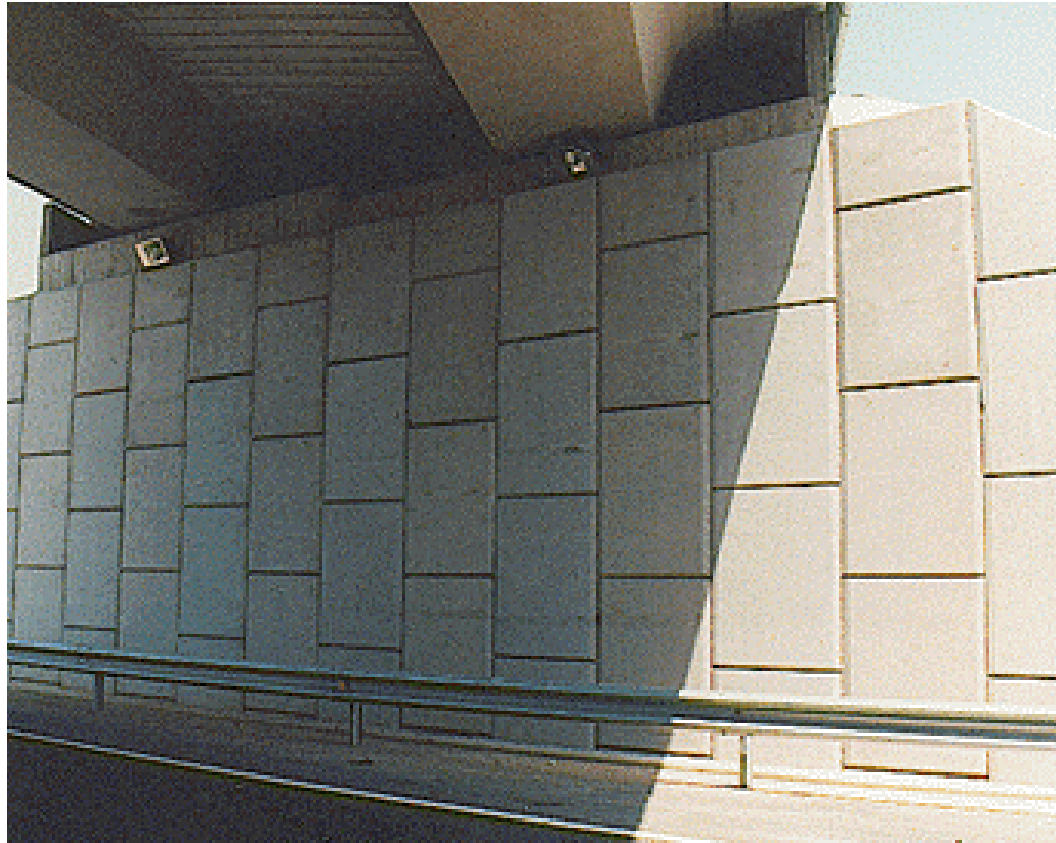
French architect and engineer
Henri **Vidal** in the early 1960s





Mechanically Stabilized Earth (MSE) Walls or Segmental Walls





Mechanically Stabilized Earth Wall (MSE Wall)



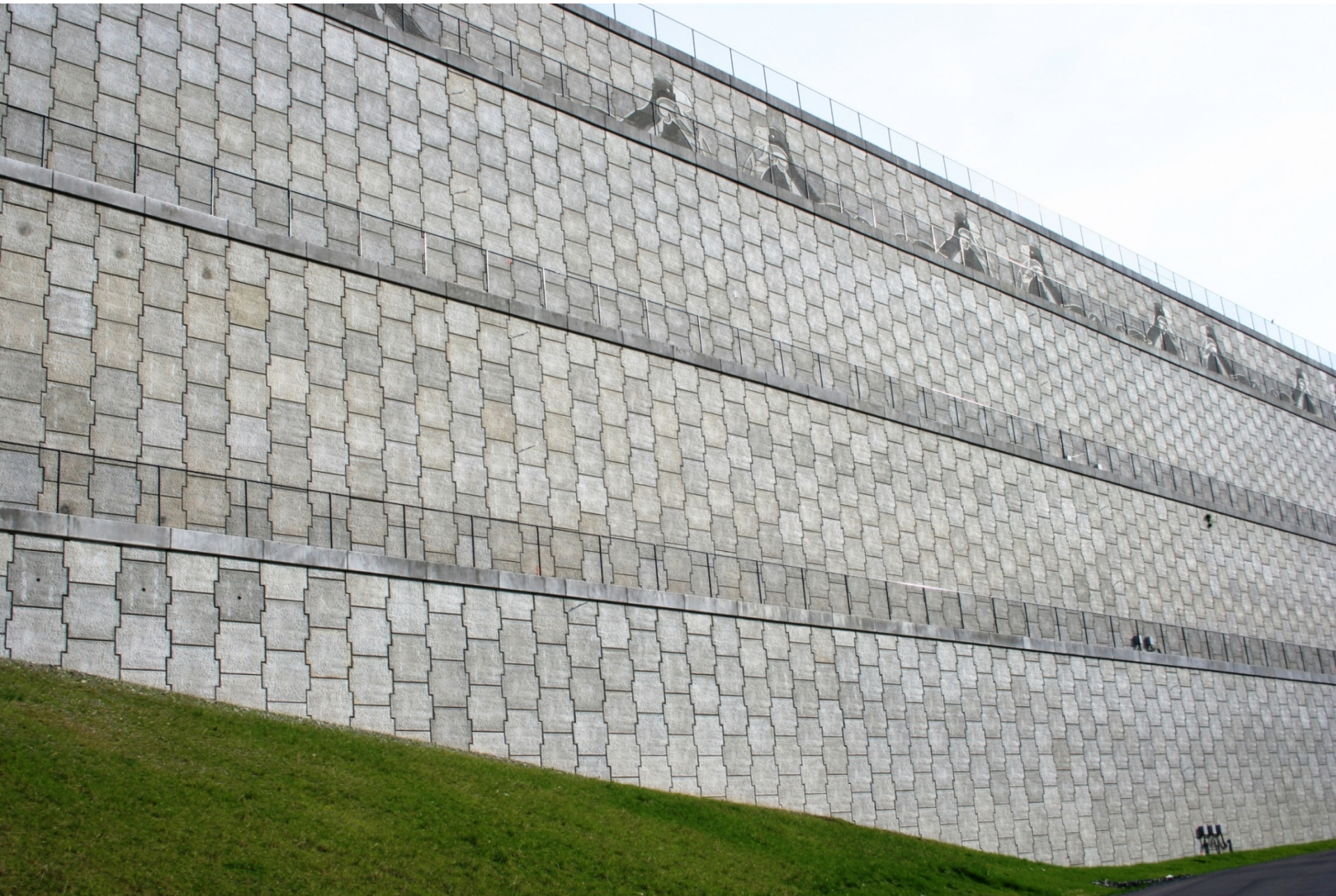


Mechanically Stabilized Earth Wall (MSE Wall)

Using Galvanized Steel



Seattle-Tacoma International Airport, WA







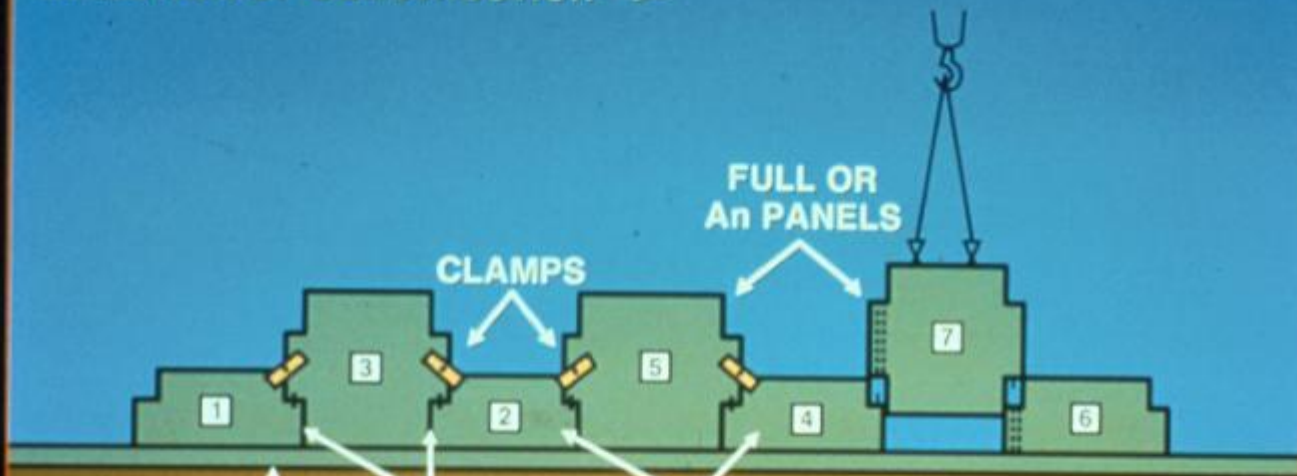








DIRECTION OF CONSTRUCTION →



CONCRETE-LEVELING PAD

HARDWOOD WEDGES

HALF OR B_n PANELS

NOTE: NUMBERS IN SQUARES SHOW ORDER OF PLACEMENT

PANEL PLACEMENT FOR INITIAL COURSE









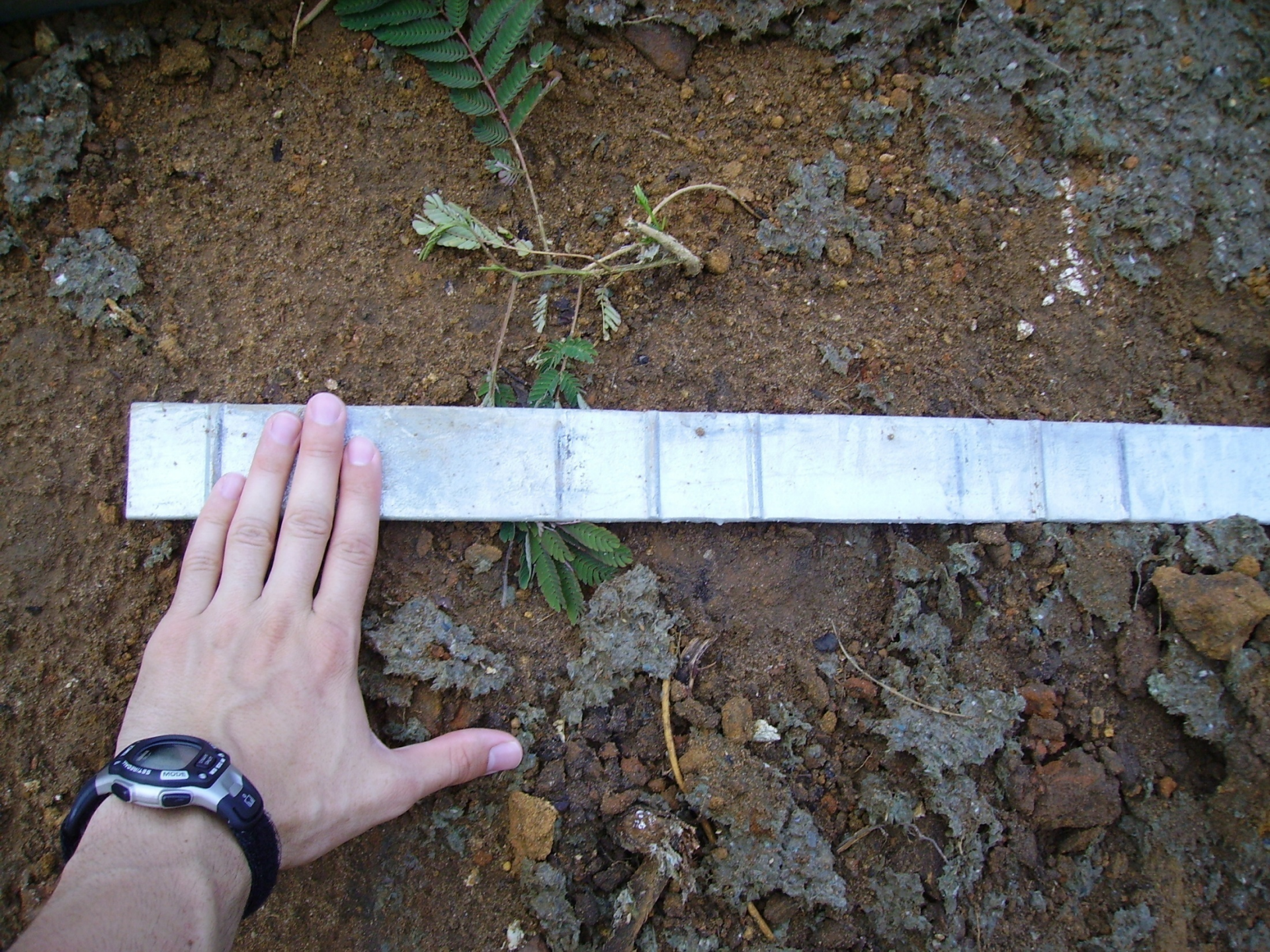








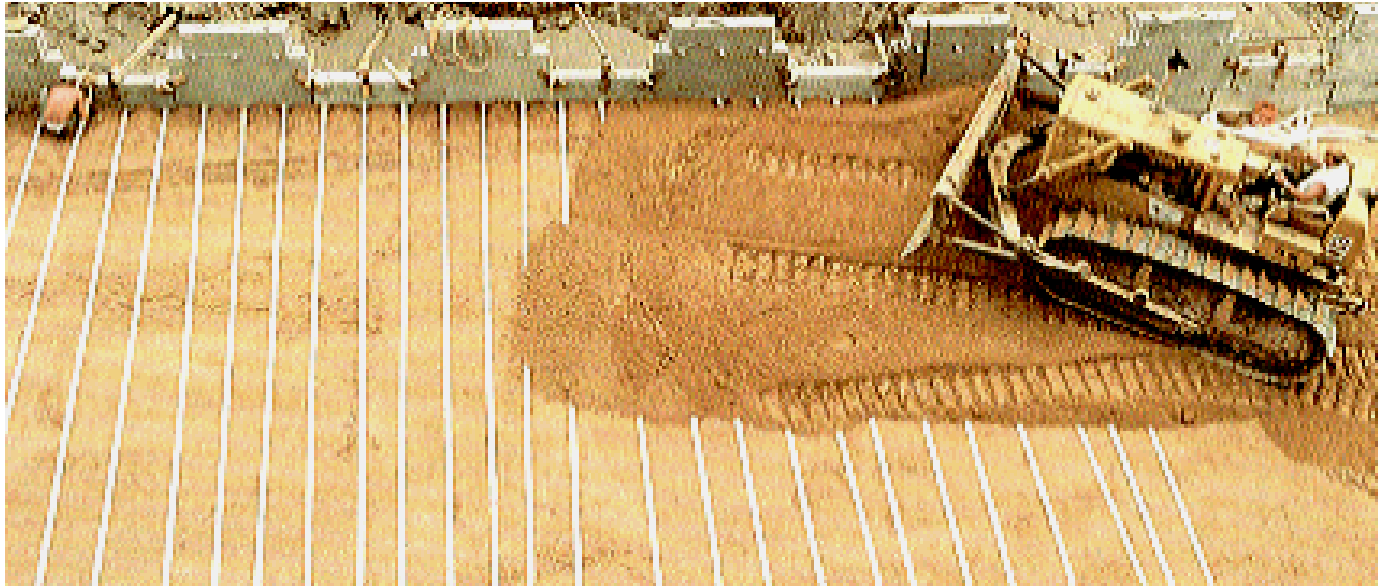










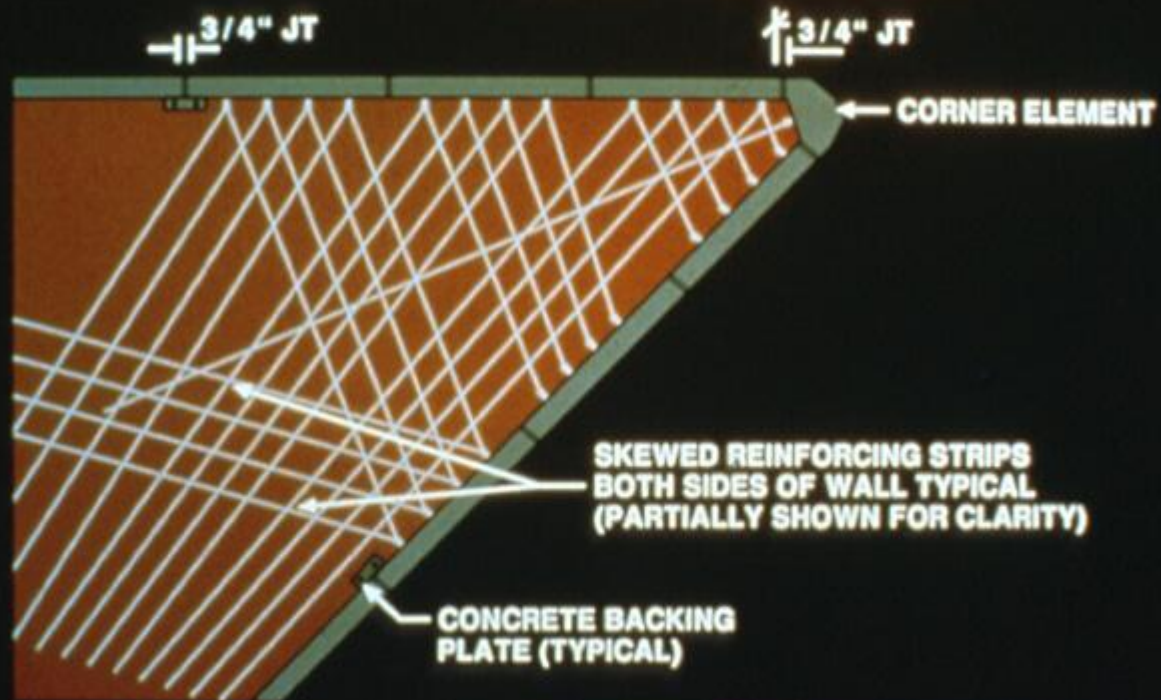


Mechanically Stabilized Earth Wall (MSE Wall)

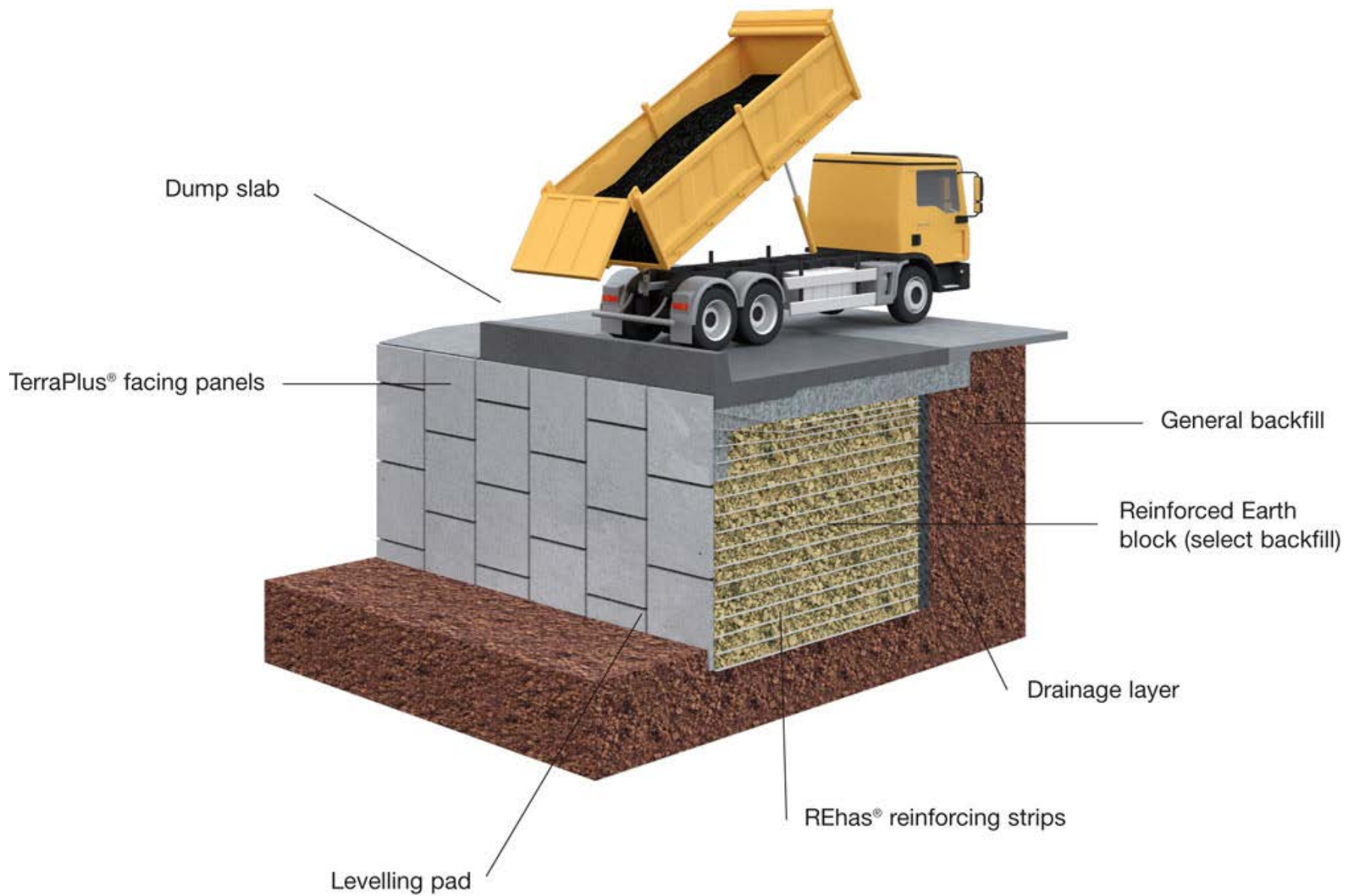




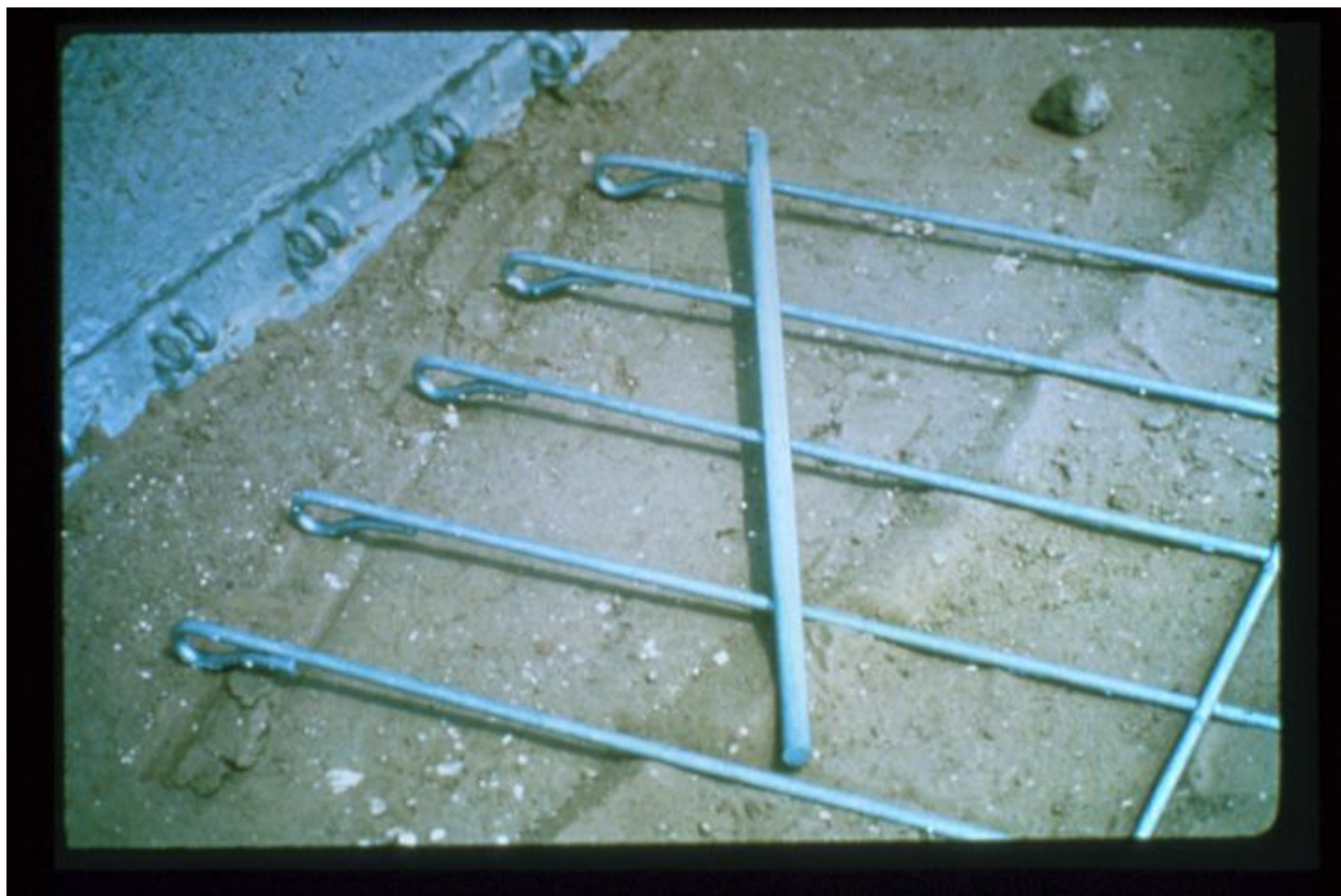
TYPICAL LAYOUT OF REINFORCING STRIPS FOR A 45° SKEW ABUTMENT





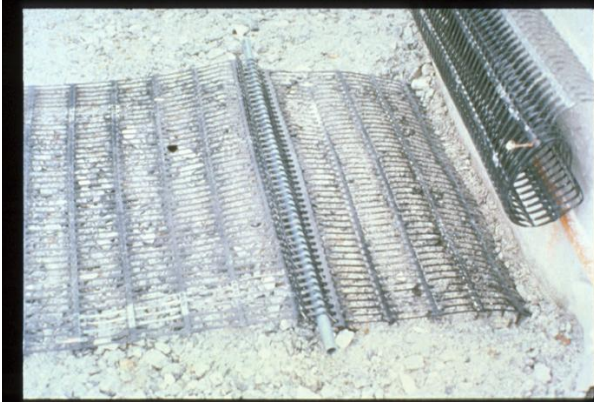








Using Geogrids





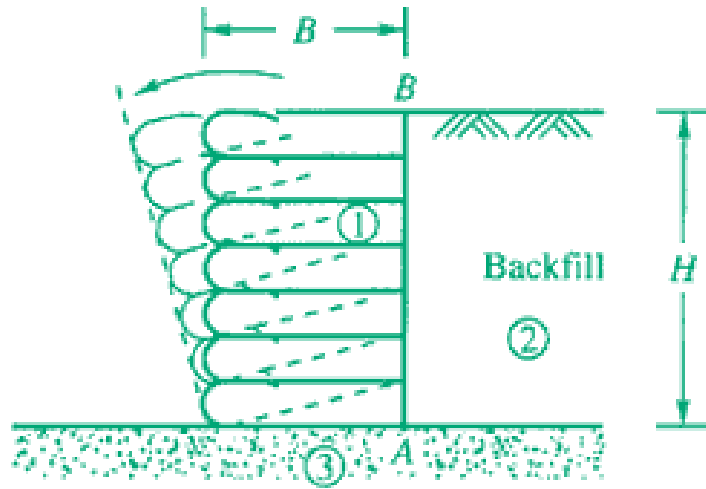


Tom Landry Highway, TX

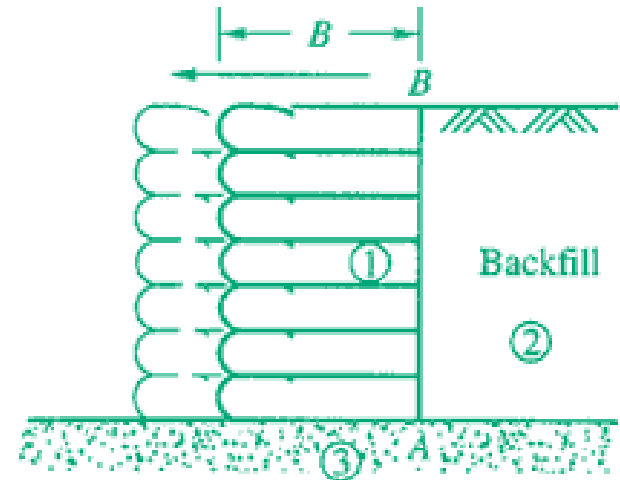


Stability of MSE Walls

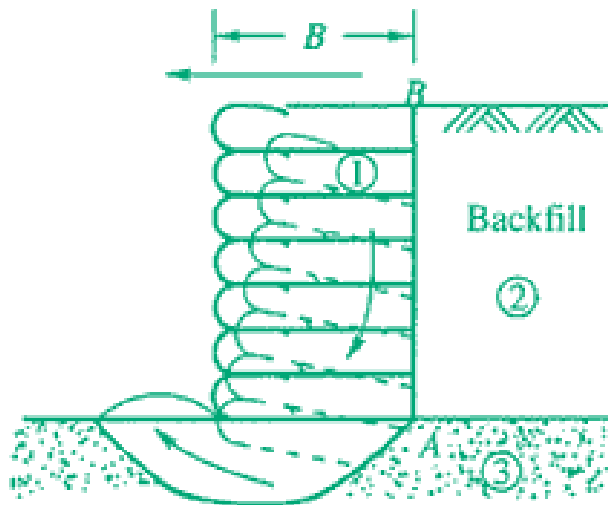
Stability of MSE Walls



(a) Overturning considerations



(b) Sliding considerations



(c) Foundation considerations

- ① Wall
- ② Backfill
- ③ Foundation soil



Block Failure



Geotechnical Design
CEG 4801
Fall 2004
By: Dr. Kamal Tawfiq



Mechanically Stabilized Earth Wall (MSE Wall)



Mechanically Stabilized Earth Wall (MSE Wall)

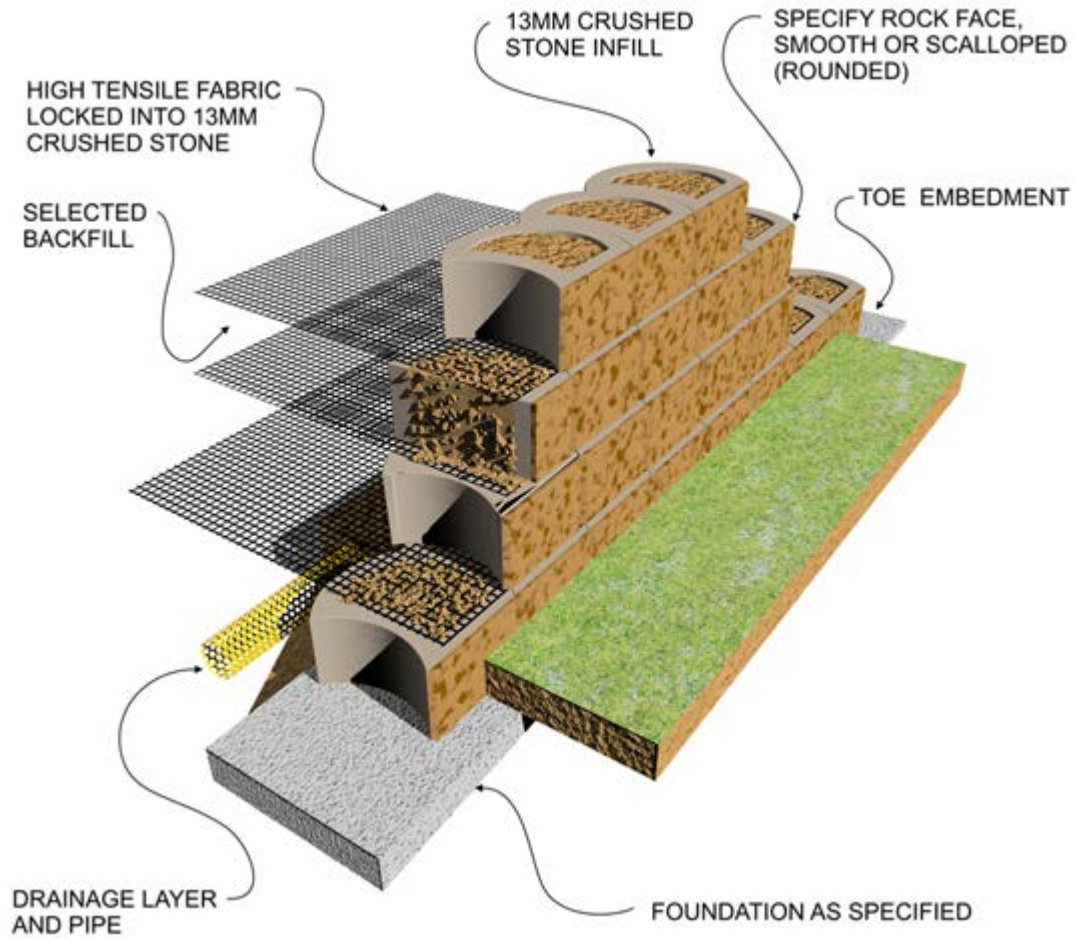
MSE Key Stone Wall

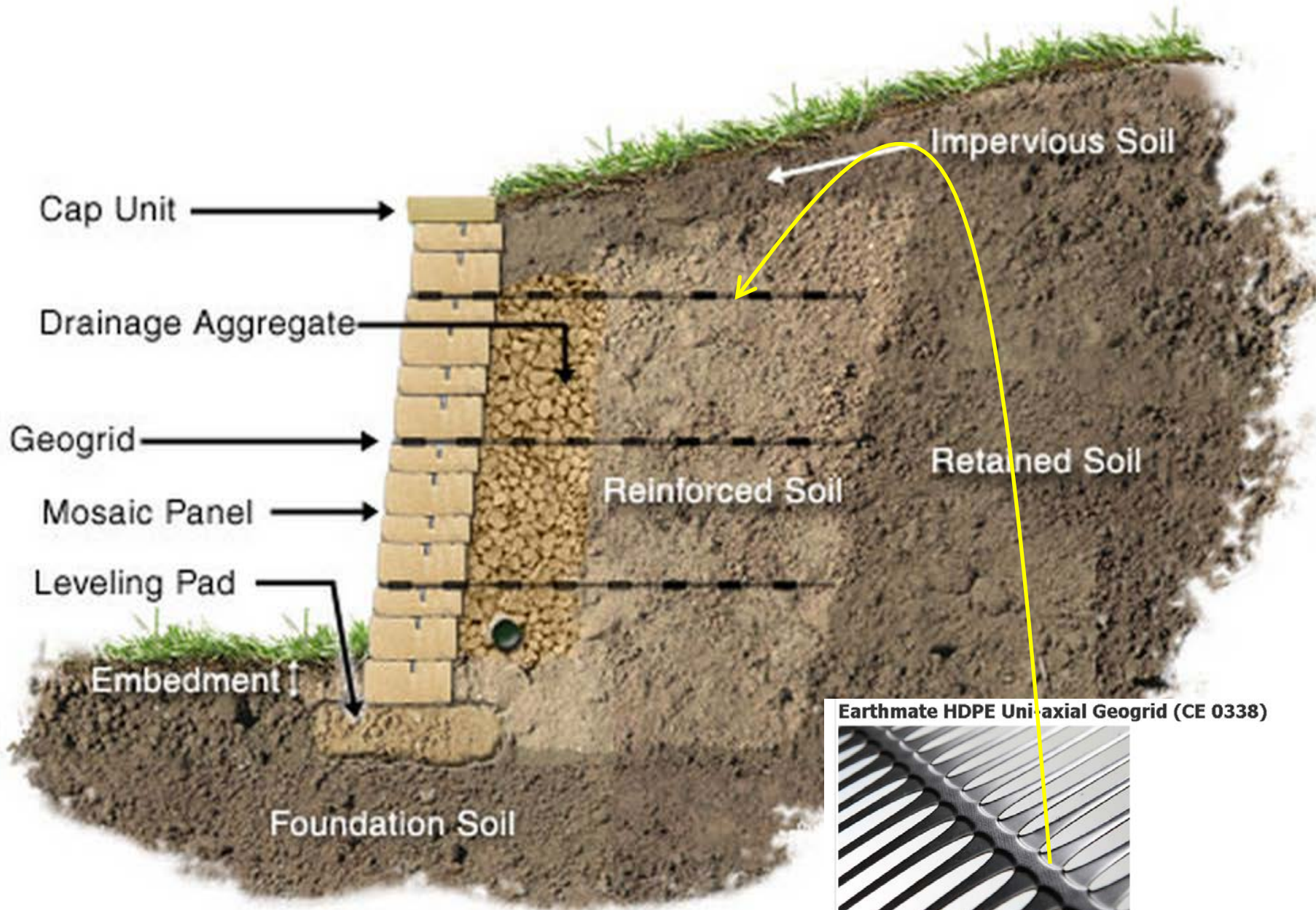
MSE Key Stone Wall





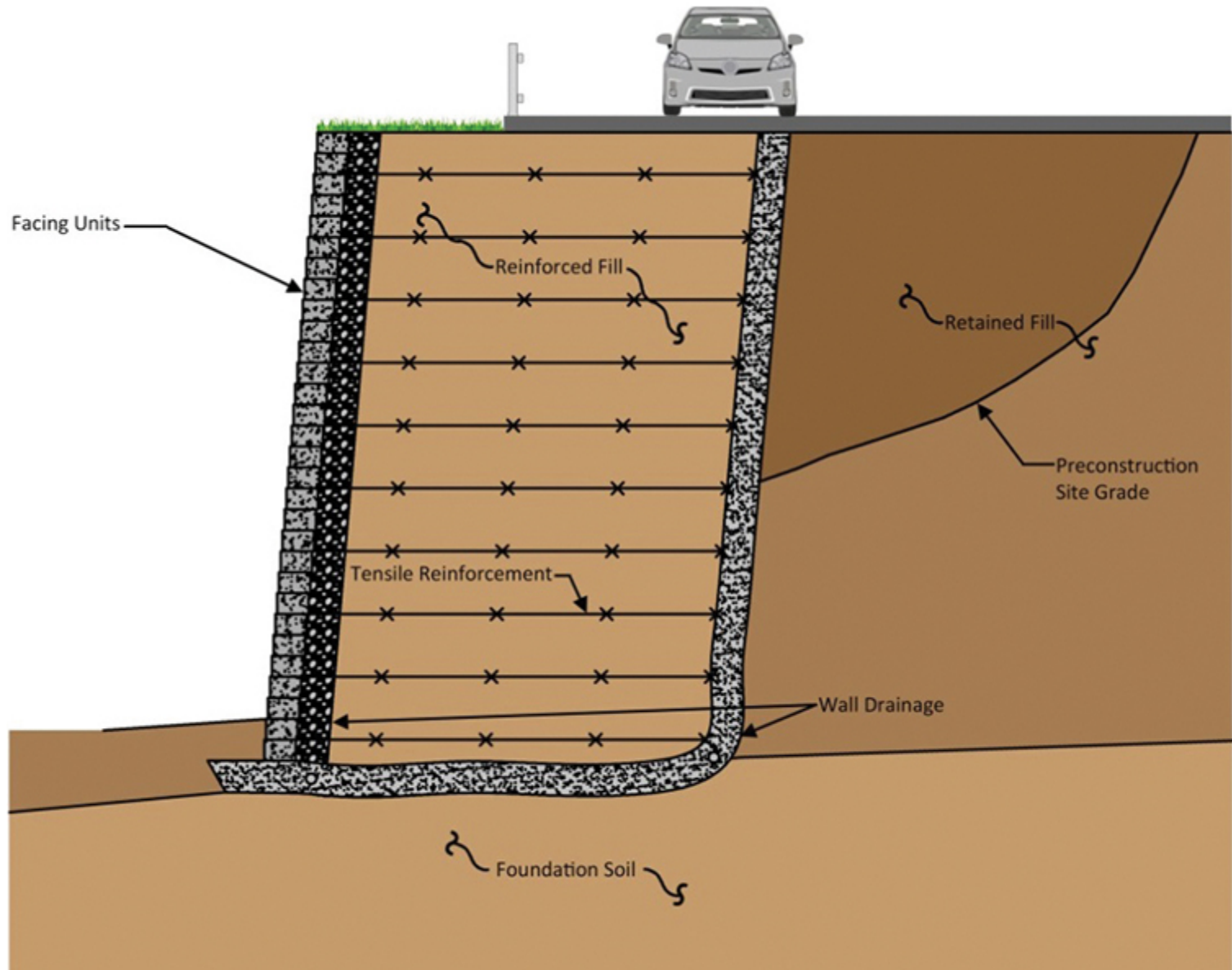


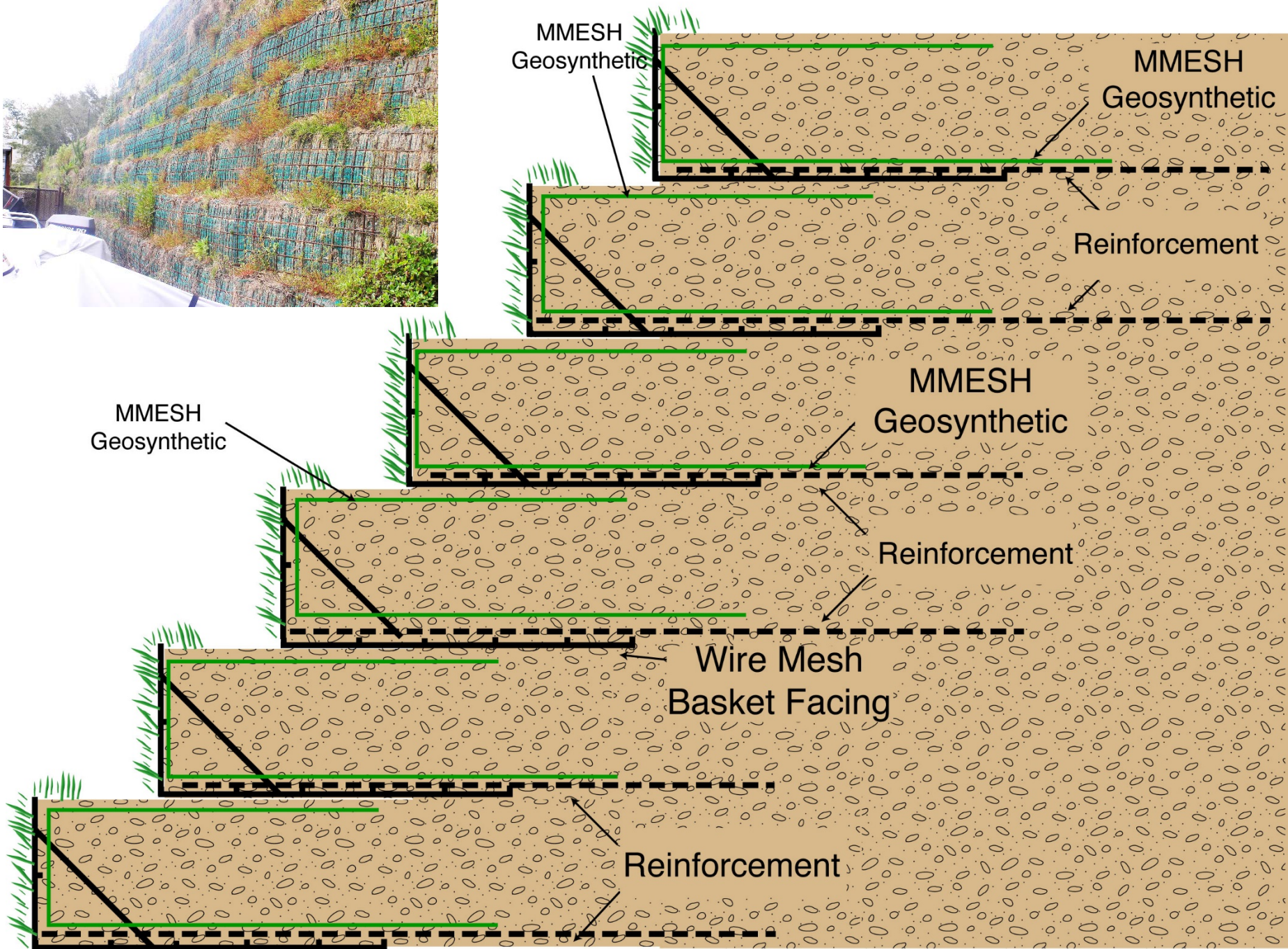




Earthmate HDPE Uni-axial Geogrid (CE 0338)

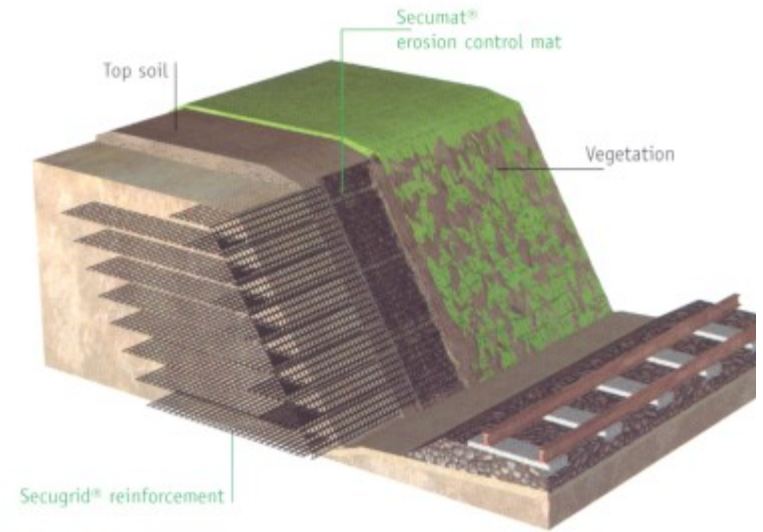
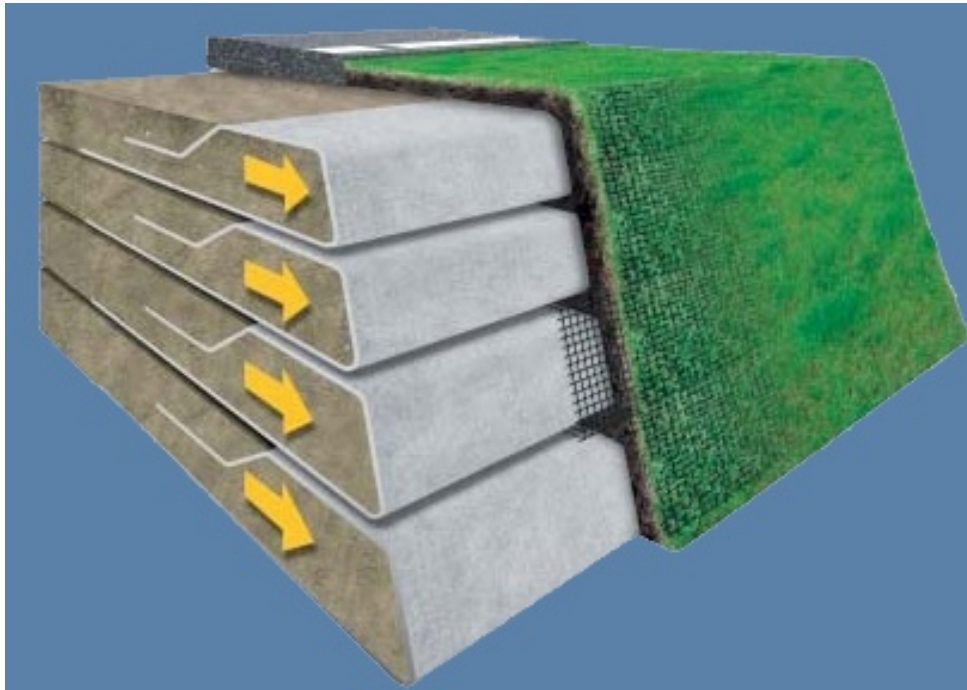








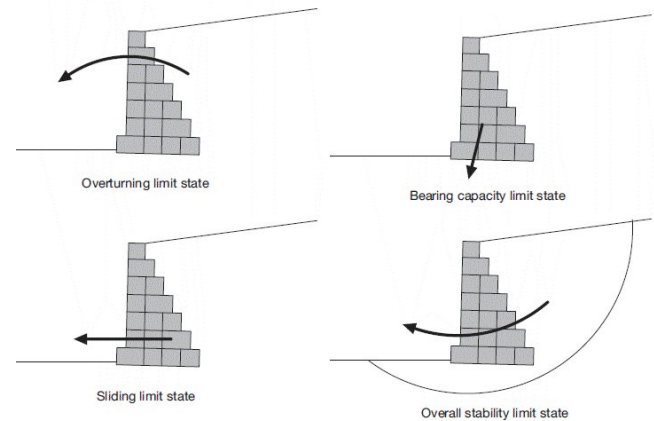
Geotextile Walls



Gabion Walls



Gabion Retaining Wall Design





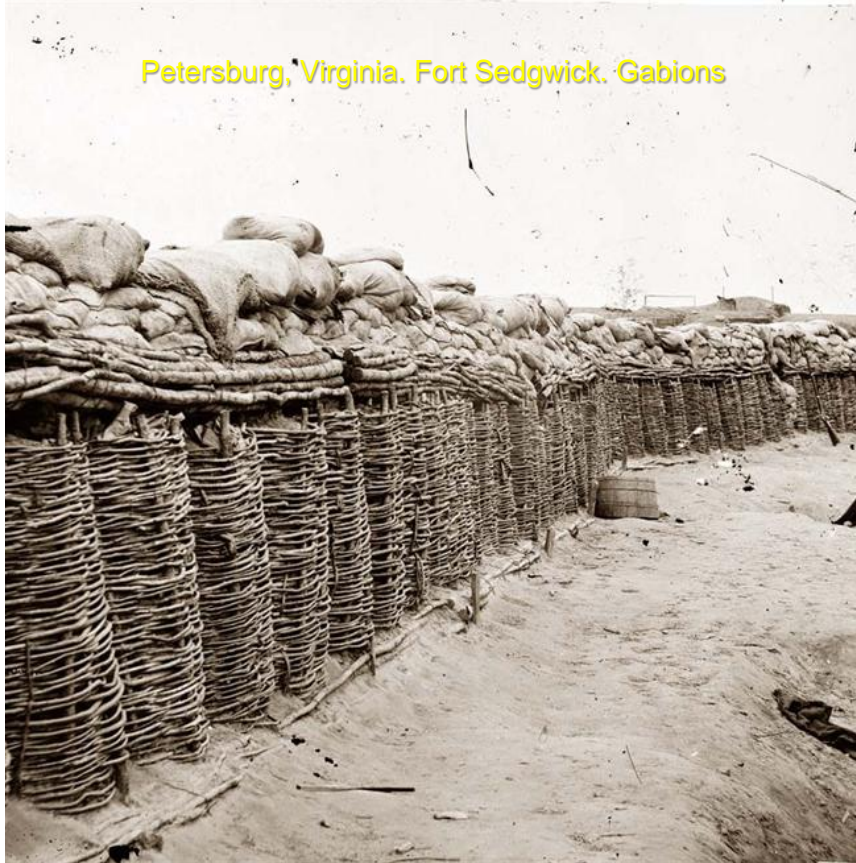
Gabion Walls

HESCO CONCERTAINER

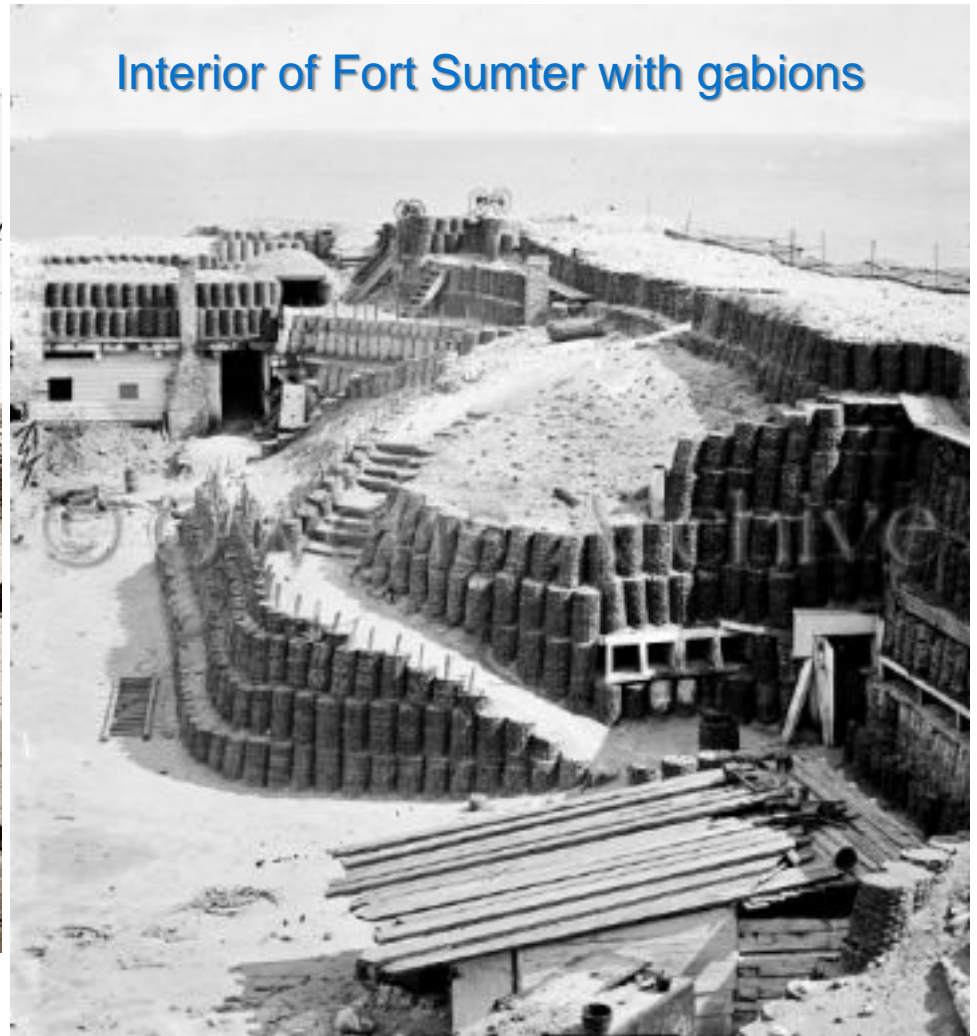
Military Accommodation Roofing, Personnel & Material Bunker Sets



Petersburg, Virginia. Fort Sedgwick. Gabions



Interior of Fort Sumter with gabions



Interior of the Union Fort Sedgwick, called by the Rebel Soldiers "Fort Hell,"
showing Union soldiers on the breastworks.
This View was taken the Morning after the storming of Petersburg, Va., April 2d, 1865.



Rebel fortifications in front of Atlanta, Georgia, in 1863 or 1864

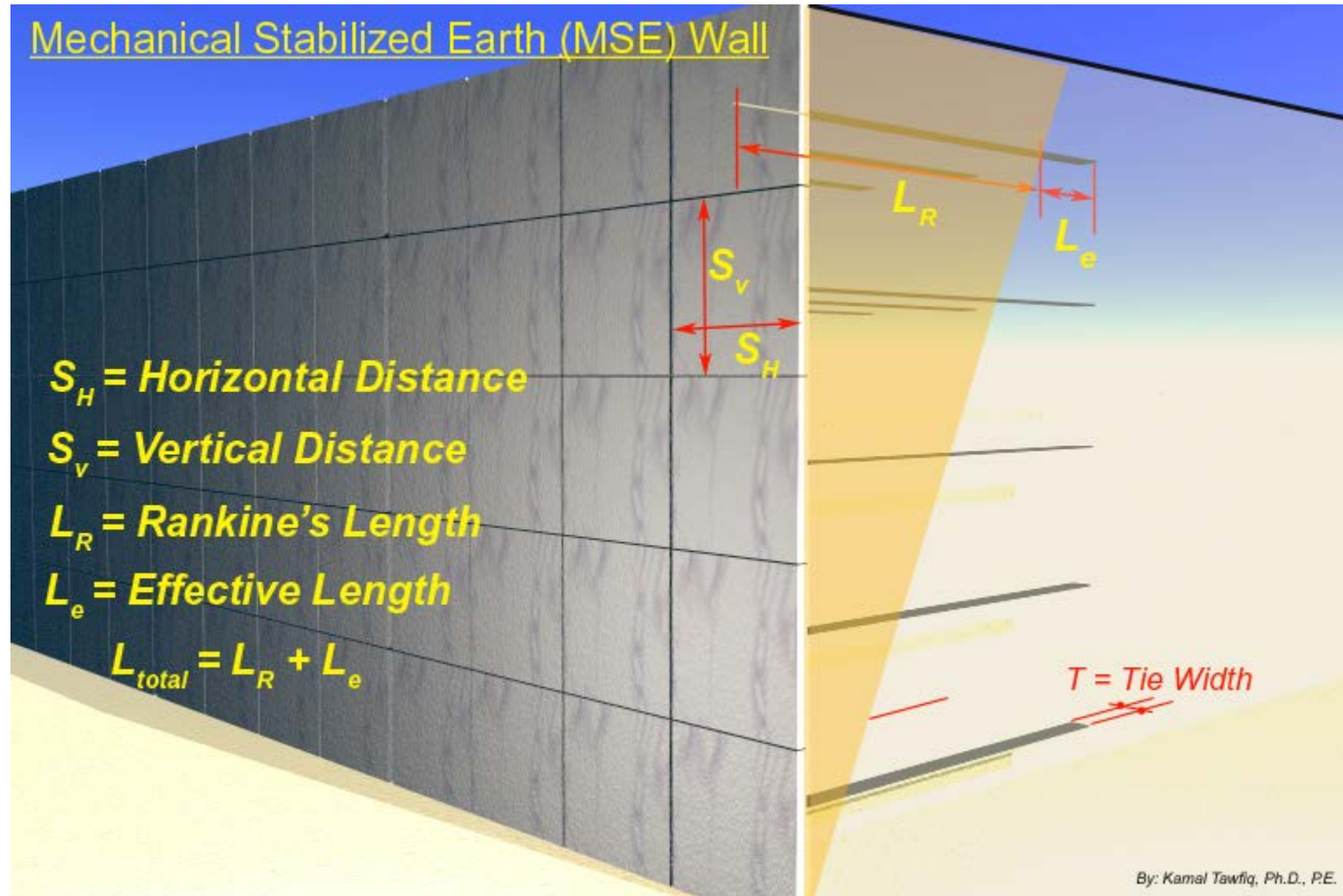


Gabions with **cannon**, from a late 16th century illustration.



MSE Wall Analysis and Design

Mechanical Stabilized Earth (MSE) Wall



A reinforced earth retaining wall is to be **30 ft high**. The properties of the backfill material are $\gamma = 110 \text{ lb/ft}^3$ and $\phi = 30^\circ$. Galvanized steel ties are to be used for the construction of the wall. Design the Reinforcements with $FS_{(B)} = 3$, $FS_{(p)} = 3$, $f_y = 29,000 \text{ psi}$ and $\phi_{tie} = 20^\circ$. The properties of the in-situ soil below the retaining wall are $\gamma = 120 \text{ lb/ft}^3$, $\phi = 30^\circ$, and $c = 150 \text{ lb/ft}^2$. Design the panels and the ties of the wall.

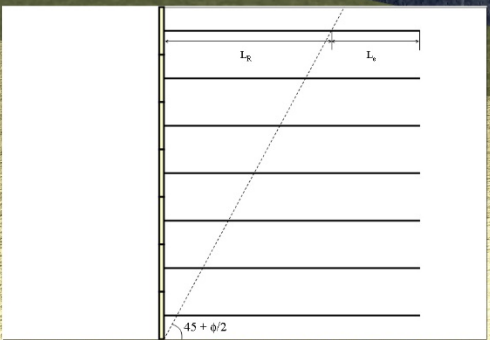
Mechanically Stabilized Earth (MSE) Wall

- $L_{total} = L_R + L_e$
- $L_R = \text{Rankine's Length}$
- $L_e = \text{Effective Length}$
- $S_H = \text{Horizontal Distance}$
- $S_v = \text{Vertical Distance}$

Tie Force = $F = \sigma_a * S_v * S_H$

FS (tie Breaking) = $\frac{w t f_y}{\sigma_a * S_v * S_H} = 2.5 \text{ to } 3$

FS (tie pullout) = $\frac{2 L_e w \sigma_v \tan \phi_H}{\sigma_a * S_v * S_H} = 2.5 \text{ to } 3$



Skin Panel

Active Wedge

L_R
 L_e

S_v
 S_H

H

$45+\phi/2$

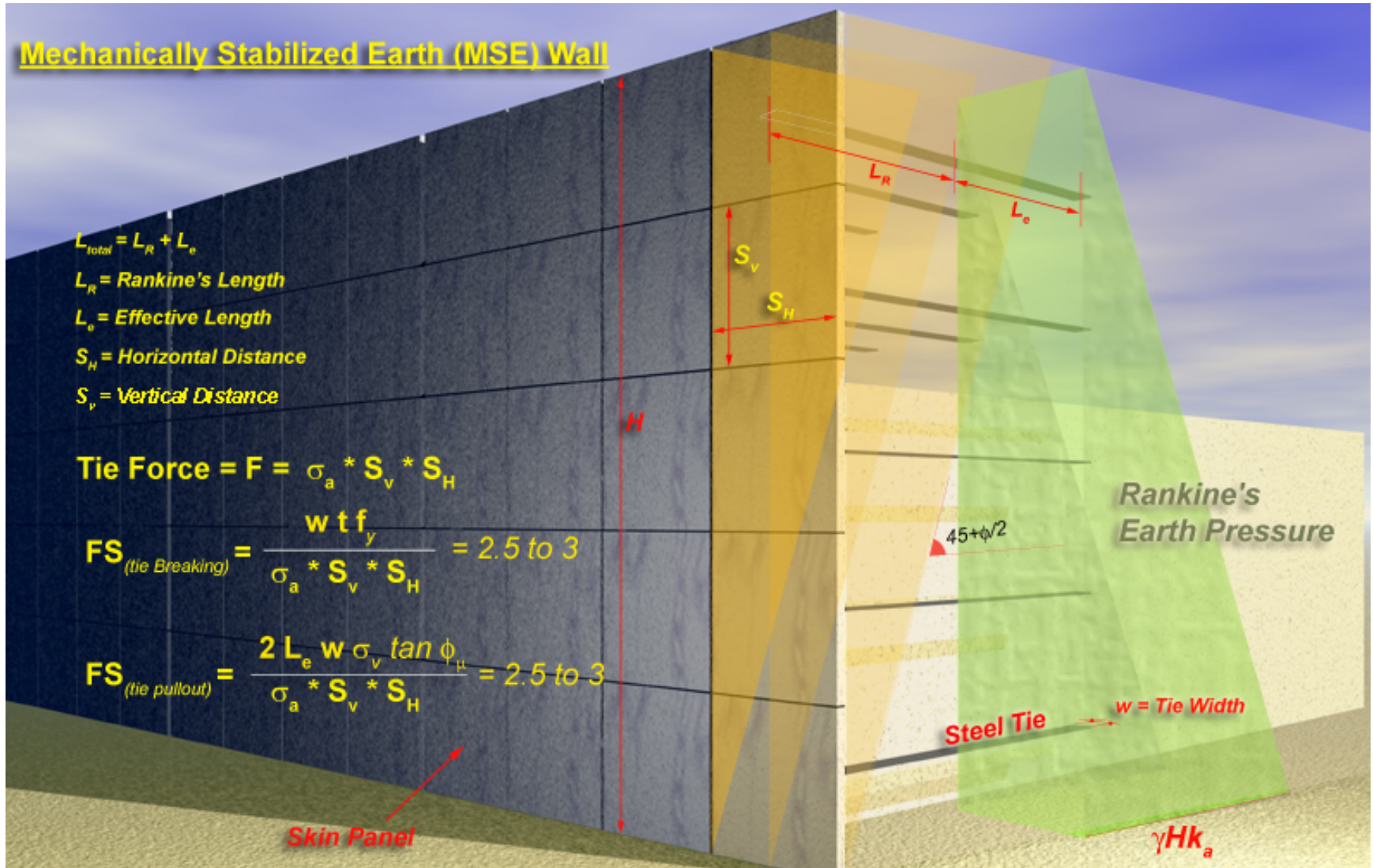
Rankine's Earth Pressure

Steel Tie
 $T = \text{Tie Width}$
 $W = \text{Tie Width}$

$\gamma H k_a$

Extend the tie beyond the active wedge to provide enough support against earth pressure of the panel

Mechanically Stabilized Earth (MSE) Wall



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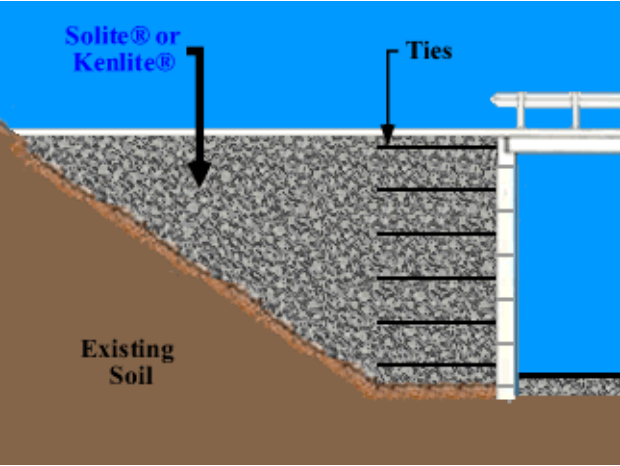
MSE Wall Project

Geotechnical Design

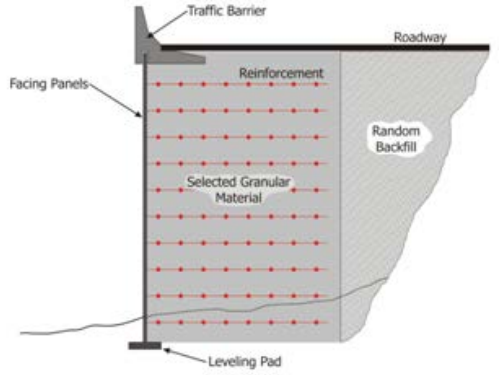
CEG 4801

Fall 2016

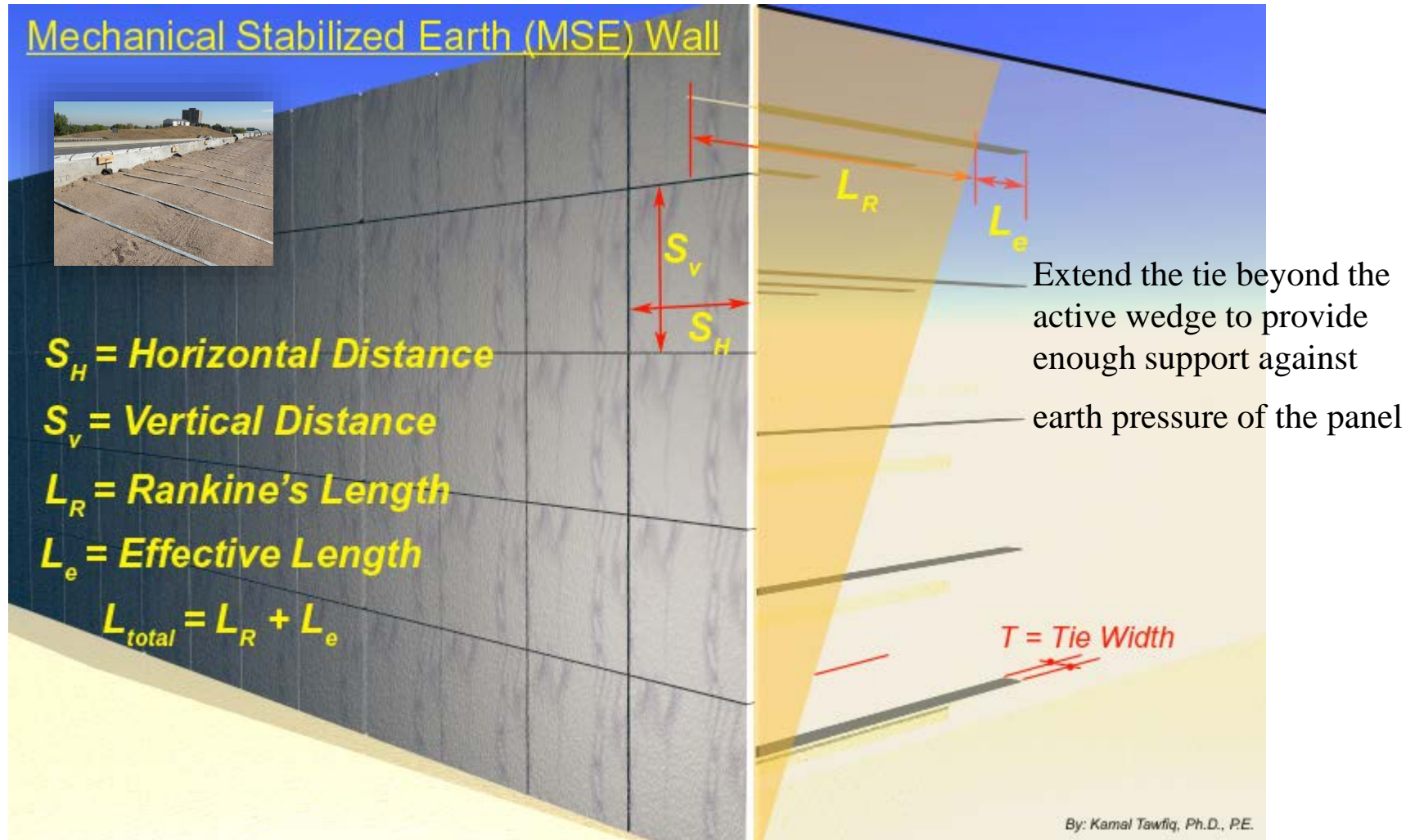
Kamal Tawfiq, Ph.D., P.E.



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Design Concept



A reinforced earth retaining wall is to be **30 ft high**. The properties of the backfill material are $\gamma = 110 \text{ lb/ft}^3$ and $\phi = 30^\circ$. Galvanized steel ties are to be used for the construction of the wall. Design the Reinforcements with $FS_{(B)} = 3$, $FS_{(p)} = 3$, $f_y = 29,000 \text{ psi}$ and $\phi_{tie} = 20^\circ$. The properties of the in-situ soil below the retaining wall are $\gamma = 120 \text{ lb/ft}^3$, $\phi = 30^\circ$, and $c = 150 \text{ lb/ft}^2$. Design the panels and the ties of the wall.

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- $L_e = \text{Effective Length}$
- $S_H = \text{Horizontal Distance}$
- $S_v = \text{Vertical Distance}$

Yield Strength of Steel H

$t = \text{thickness of tie}$

Tie Force = $F = \sigma_a * S_v * S_H$

$FS_{(tie\ breaking)} = \frac{w t f_y}{\sigma_a * S_v * S_H} = 2.5 \text{ to } 3$

Friction angle between steel and soil (given)

$FS_{(tie\ pullout)} = \frac{2 L_e w \sigma_v \tan \phi_H}{\sigma_a * S_v * S_H} = 2.5 \text{ to } 3$

Skin Panel

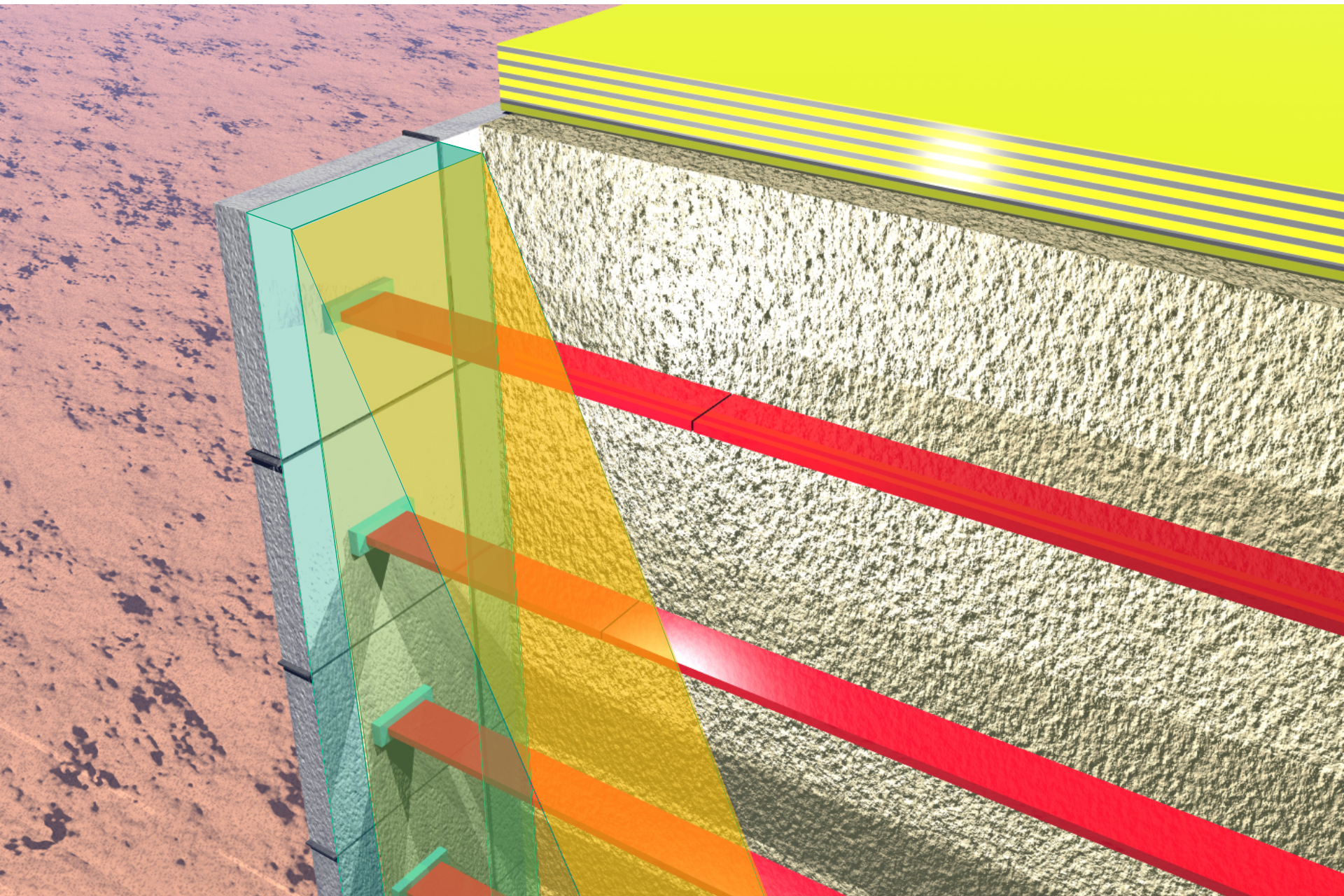
Steel Tie

$w = \text{Tie Width}$

$\gamma H k_a$

Rankine's Earth Pressure

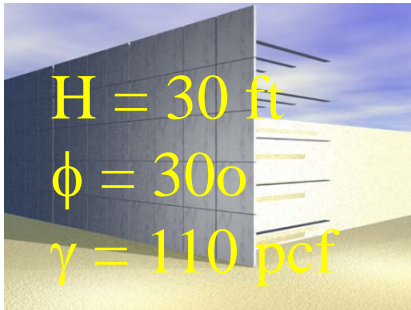
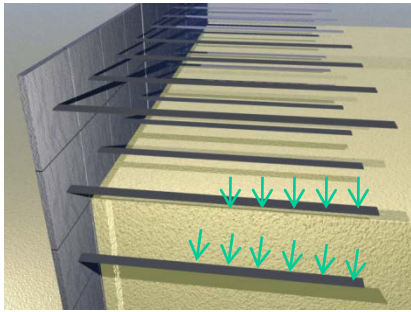
$45 + \phi/2$



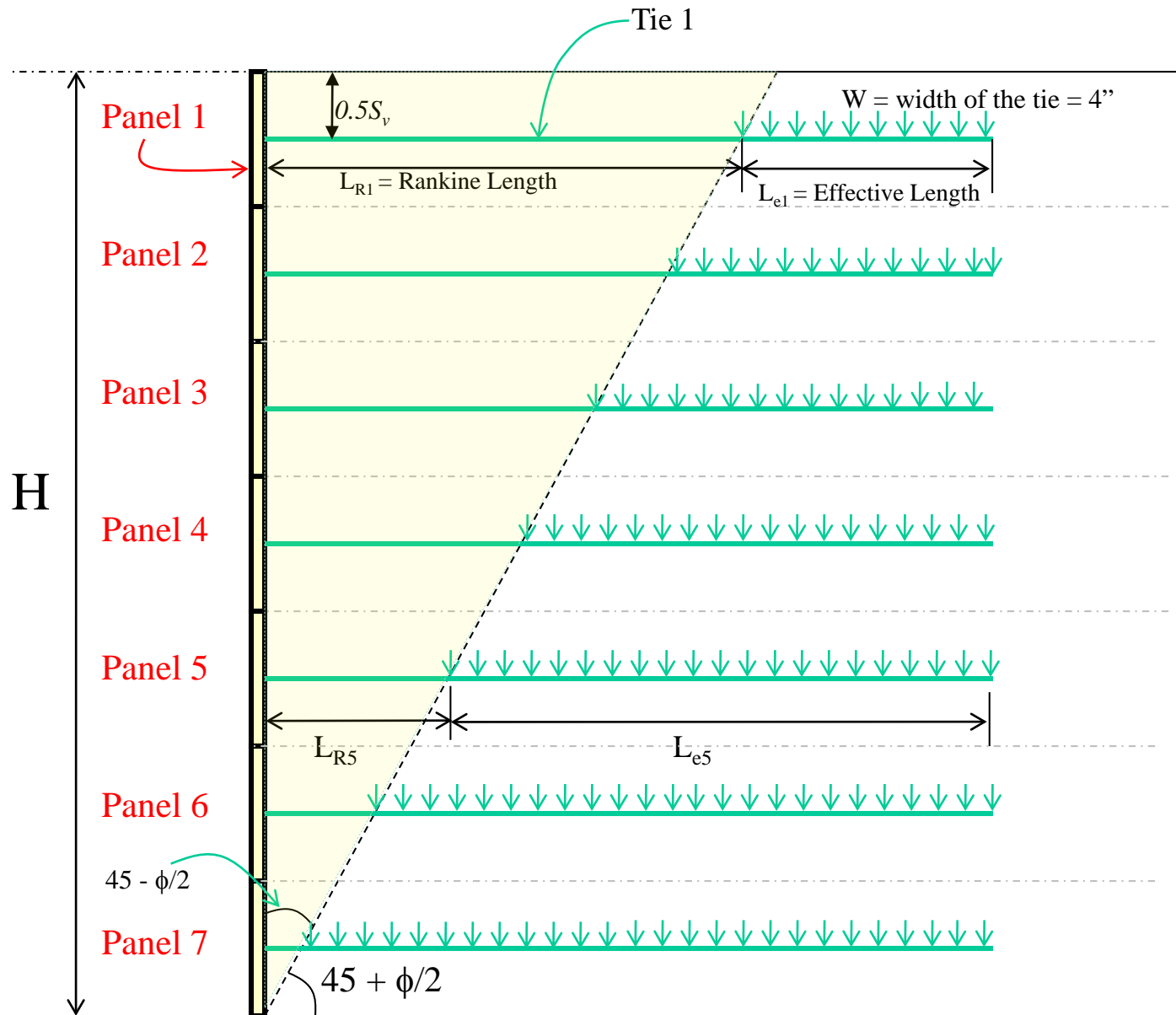
$$L_{R1} = (H - 0.5 S_v) \tan (45 - \phi/2)$$

$$L_{e1} = \frac{2.5(\sigma_a \cdot S_v \cdot S_H)}{2 w \sigma_v \tan \phi_\mu}$$

$$L_1 = L_{R1} + L_{e1}$$



H

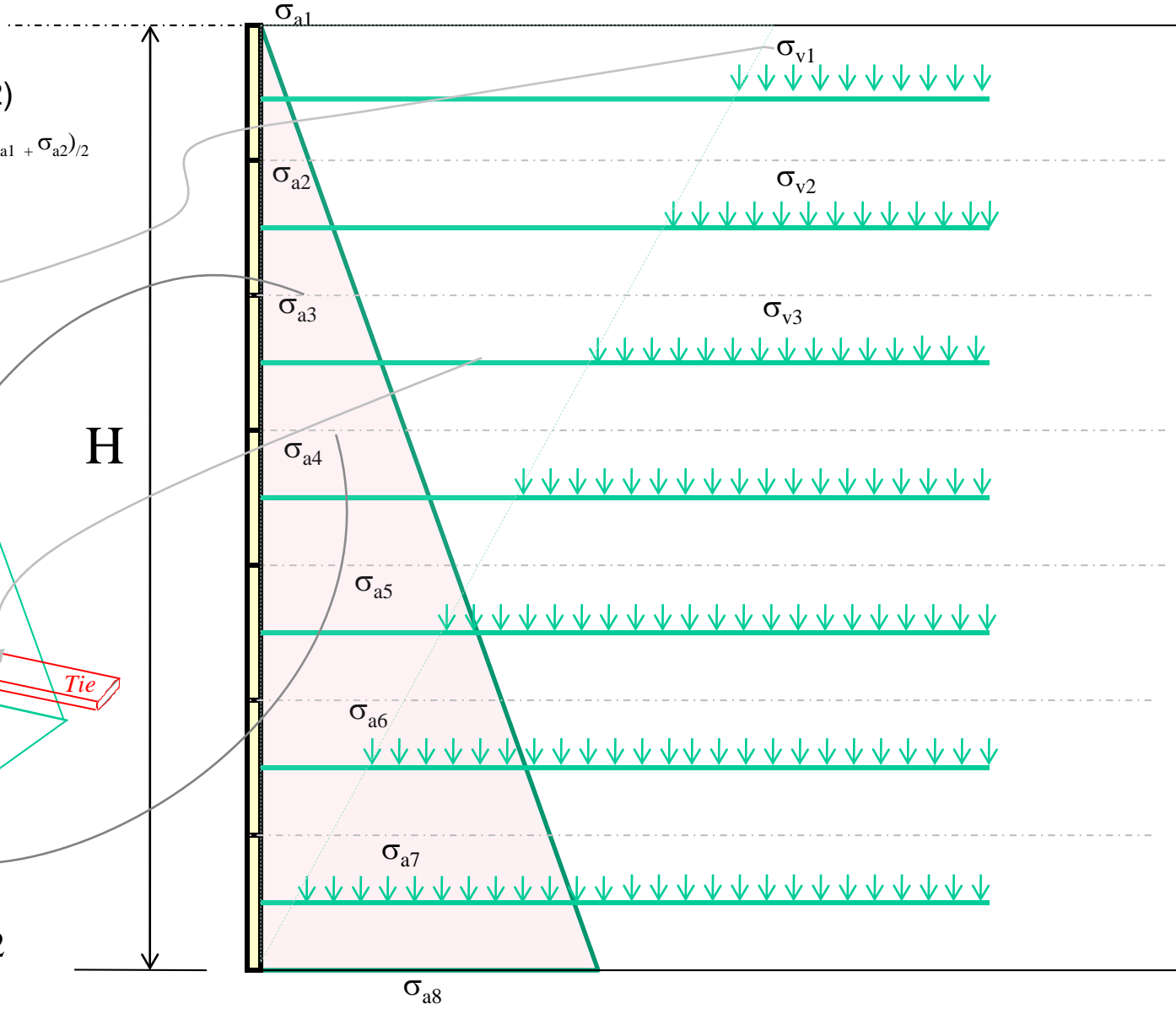
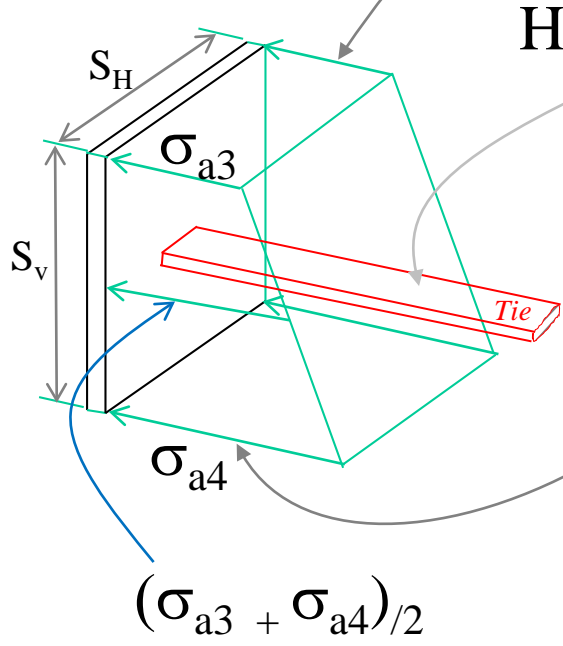


$$L_{R1} = (H - 0.5 S_v) \tan(45 - \phi/2)$$

$$L_{e1} = \frac{2.5(\sigma_a \cdot S_v \cdot S_H)}{2 w \sigma_v \tan \phi_\mu}$$

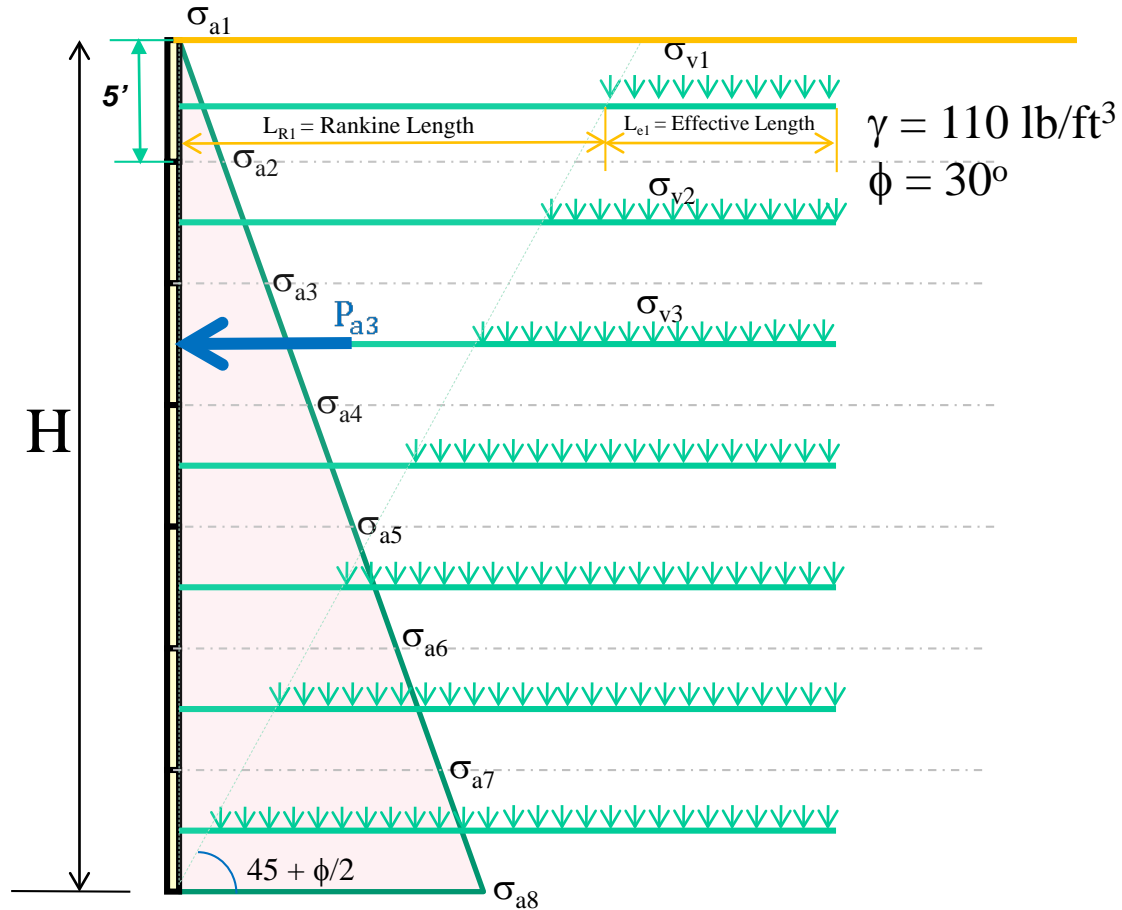
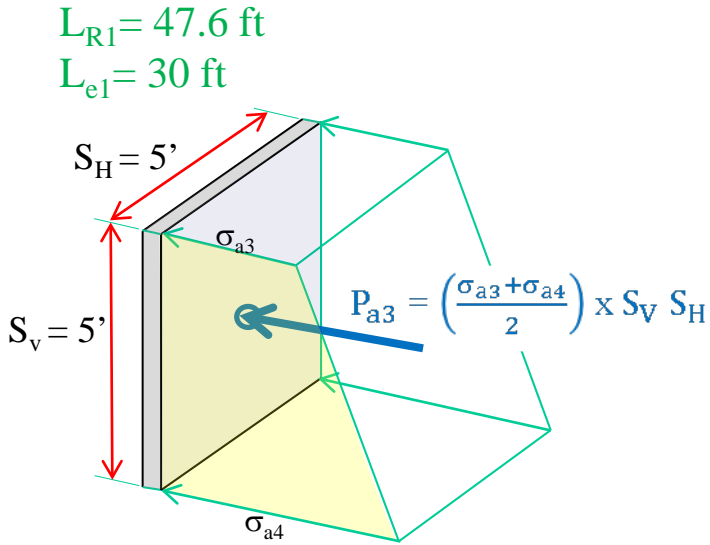
$(\sigma_{a1} + \sigma_{a2})/2$
 Tie width

$$L_1 = L_{R1} + L_{e1}$$



Example:

A reinforced earth retaining wall is to be **30 ft high**. The properties of the backfill material are $\gamma = 110 \text{ lb/ft}^3$ and $\phi = 30^\circ$. Galvanized steel ties are to be used for the construction of the wall. Design the Reinforcements with $FS_{(B)} = 3$, $FS_{(p)} = 3$, $f_y = 29,000 \text{ psi}$ and $\phi_{\text{tie}} = 20^\circ$. The properties of the in-situ soil below the retaining wall are $\gamma = 120 \text{ lb/ft}^3$, $\phi = 30^\circ$, and $c = 150 \text{ lb/ft}^2$. Design the panels and the ties of the wall.



Solution:

$$k_a = \frac{1 - \sin \phi}{1 + \sin \phi} = \frac{1 - \sin 30}{1 + \sin 30} = 0.33$$

Point	Tie	Depth (ft)	Vertical Stress (σ_v) lb/ft ²	Horizontal Stress (σ_a) lb/ft ²	$\sigma_a \cdot S_v \cdot S_H$	$\sigma_v \cdot \tan \phi_m$	L_e	L_R	L_{total}	$t = \frac{\sigma_a \cdot S_v \cdot S_H}{S_H/w \cdot f_y}$
1		0	0	0						
	Tie 1	2.5	275	90.75	2268.75	100.09	102.0	47.63	150	0.058675
2		5	550	181.5						
	Tie 2	7.5	825	272.25	6806.25	300.28	102.0	38.97	141	0.176024
3		10	1100	363						
	Tie 3	12.5	1375	453.75	11343.75	500.46	102.0	30.31	132	0.293373
4		15	1650	544.5						
	Tie 4	17.5	1925	635.25	15881.25	700.64	102.0	21.65	124	0.410722
5		20	2200	726						
	Tie 5	22.5	2475	816.75	20418.75	900.83	102.0	12.99	115	0.528071
6		25	2750	907.5						
	Tie 6	27.5	3025	998.25	24956.25	1101.01	102.0	4.33	106	0.645420
7		30	3300	1089						

